

CRES Control Using CDA as a Shielding Gas

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Outline

- Background – the journey
- Problem Statement
- Measurement/Methodology
- Key Findings
- Solution's
- Acknowledgments

Background

- Factory Expansion Phase 4 – just completed
- Phase 4 automotive factory was experiencing significant CRes yield loss issues between testers and devices
- Phase 5 to ramping ~ 150 systems migrating to automotive 3 insertion test methodology

Problem Statement

- Factory was experiencing significant CRes yield loss issues between testers and devices during 3 insertion probing sequence at different temps
- CRes fails were causing significant yield loss and requiring significant reprobe time losses
- Traditional CRes solutions were reaching the limits of effectiveness

Objective

- Show the effects of CDA on CRes
- Review the potential impact of CDA that effect die temperature
- Review design/hardware procedures needed to manage CDA
- Share key learning's – the journey

CRes Sources Probe

~~Bond Pad Surface~~

~~Test Program~~

~~Diode Structure~~

~~PC Planarity~~

~~Cleaning Frequency~~

~~Debris Field~~

~~Test Head Level~~

~~Z-Axis Travel~~

~~Chuck Speed~~

~~Muffin Fans~~

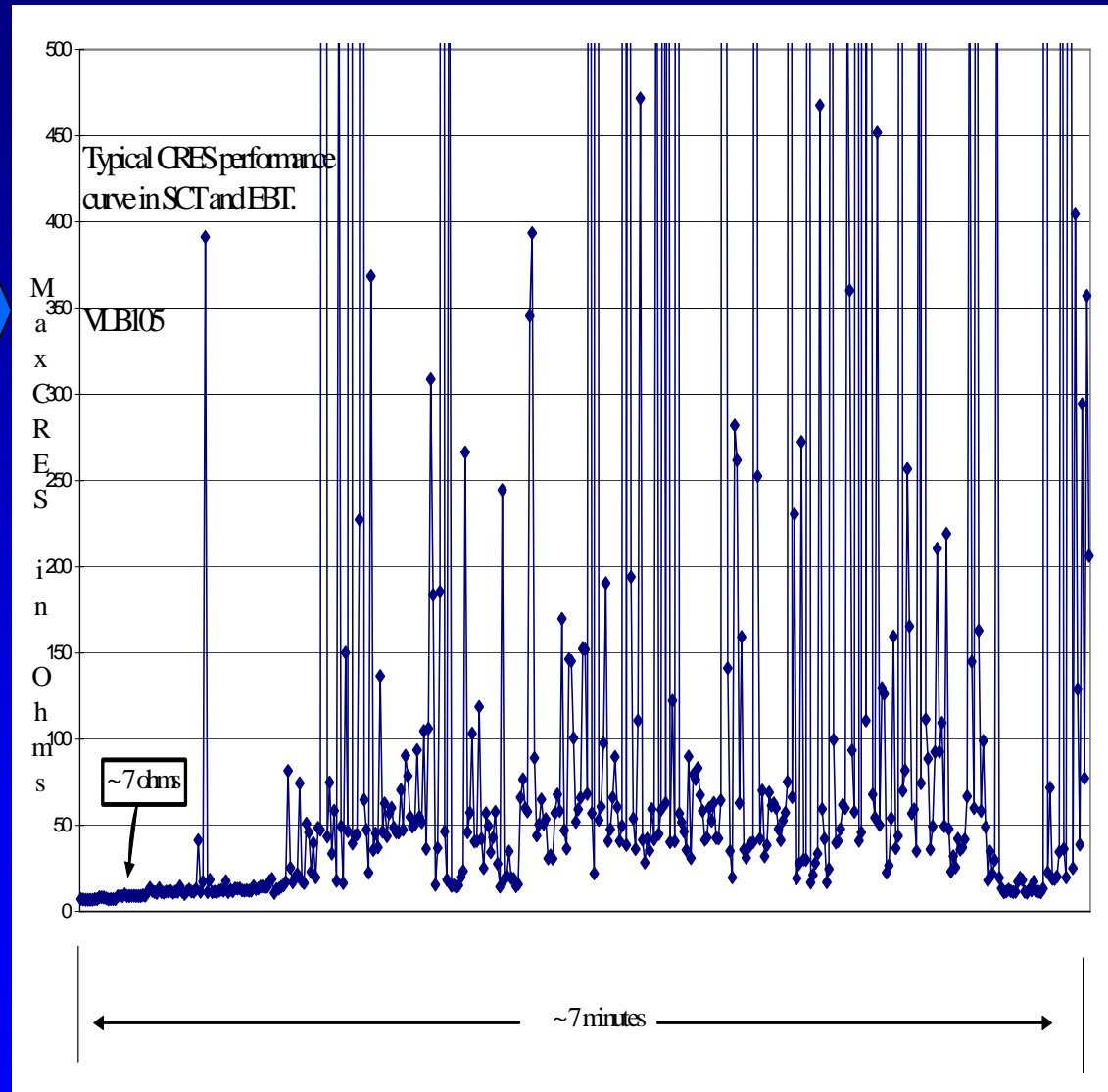
~~Air Handlers~~

~~Raised Floor~~

~~Equipment Density~~

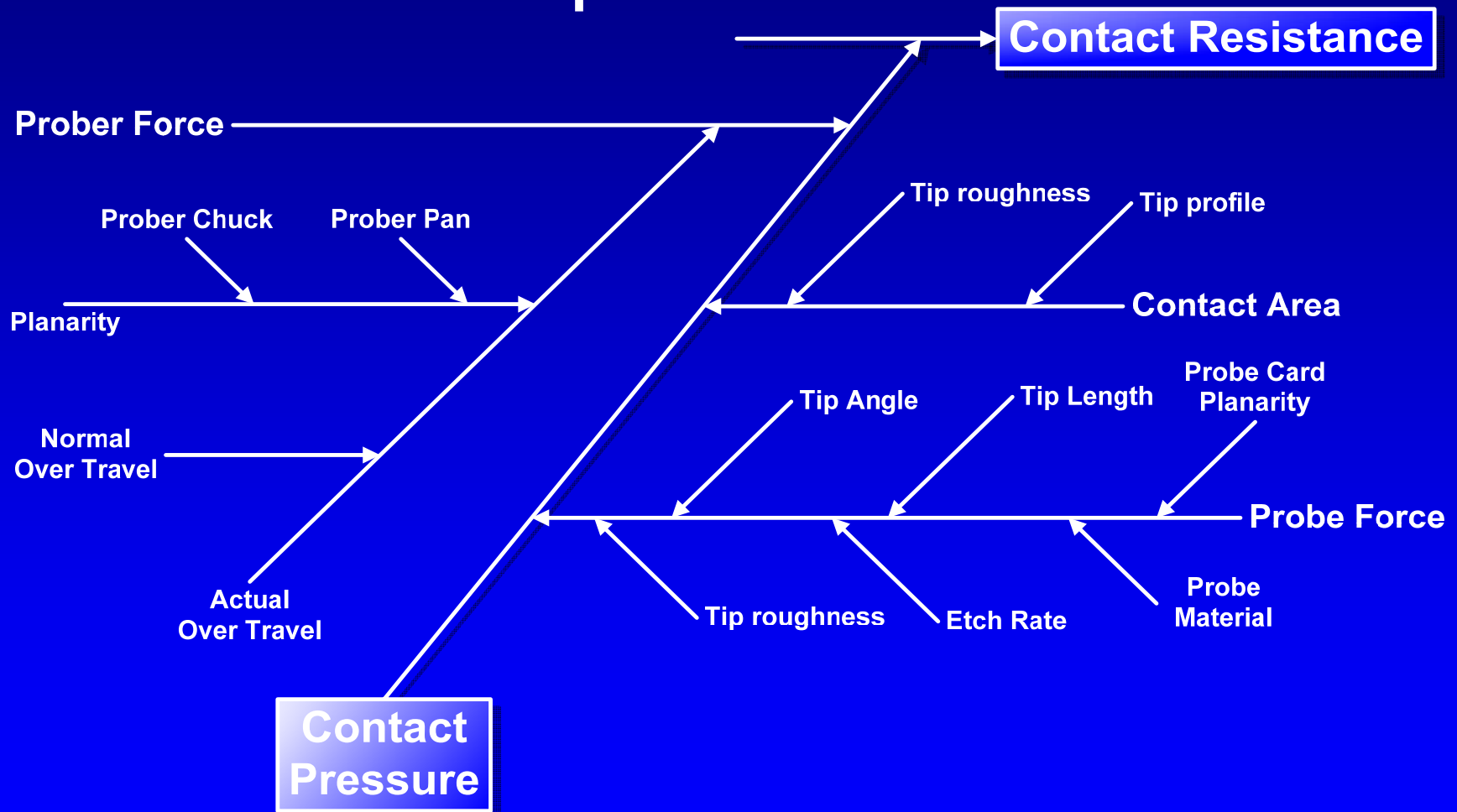
H₂O ?

Conditions
that effect
CRes

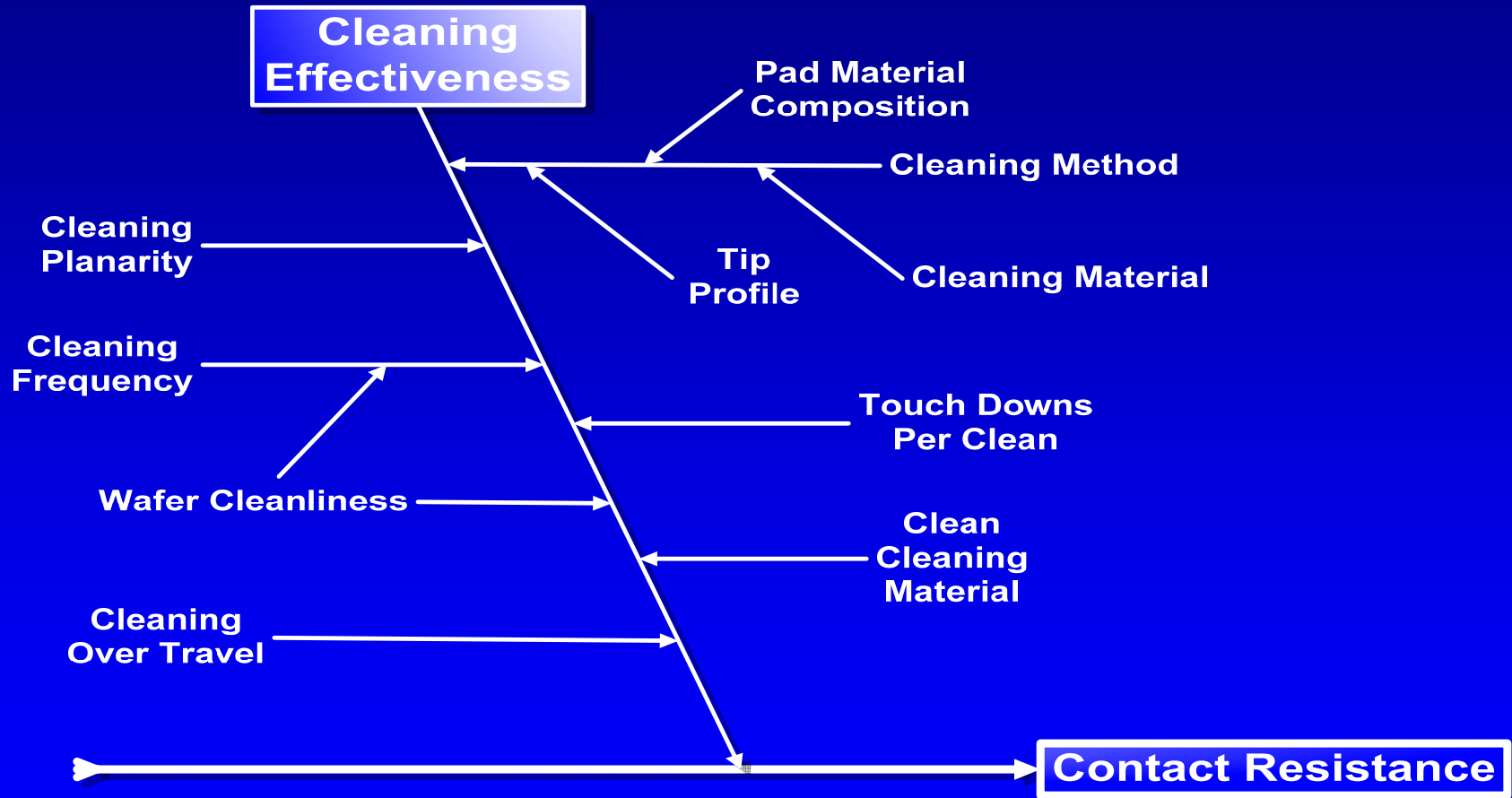


Cres Causes by Category

Nearly all are out of the control of operations



Cleaning Frequency change most common approach to control CRES at probe.



Cleaning Effectiveness

- A Paradigm Shift

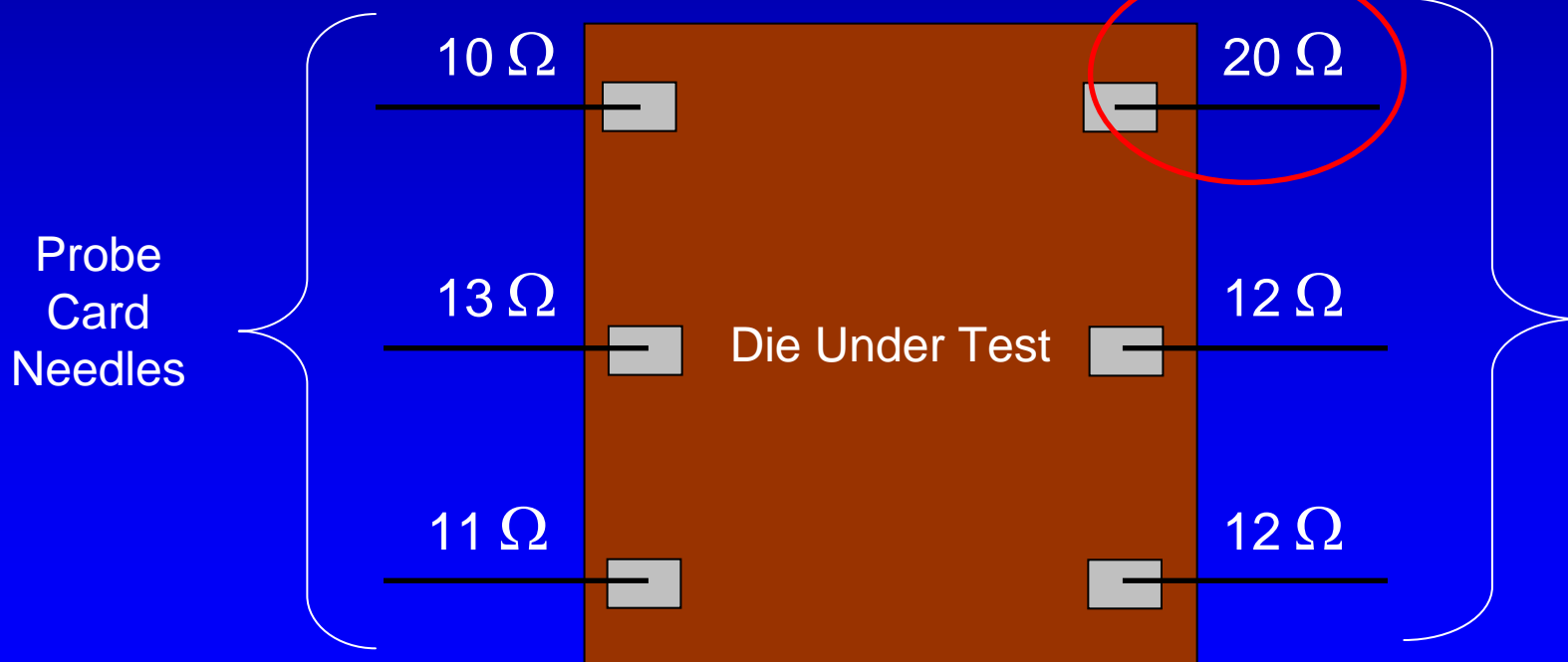
- Improving Contact Resistance without Increasing on-line Cleaning?

- Injecting Compressed Dry Air (CDA) on the Die Under Test has improved the stability of CRES and reduces the need for additional on-line cleaning

Discovery Experiments

- Blanket Aluminum Wafer
- Cantilever Dual-Site Probe Card
- VLCLT Tester
- CDA
- Nitrogen
- Maximum Contact Resistance (MAXCRES) used to plot effects

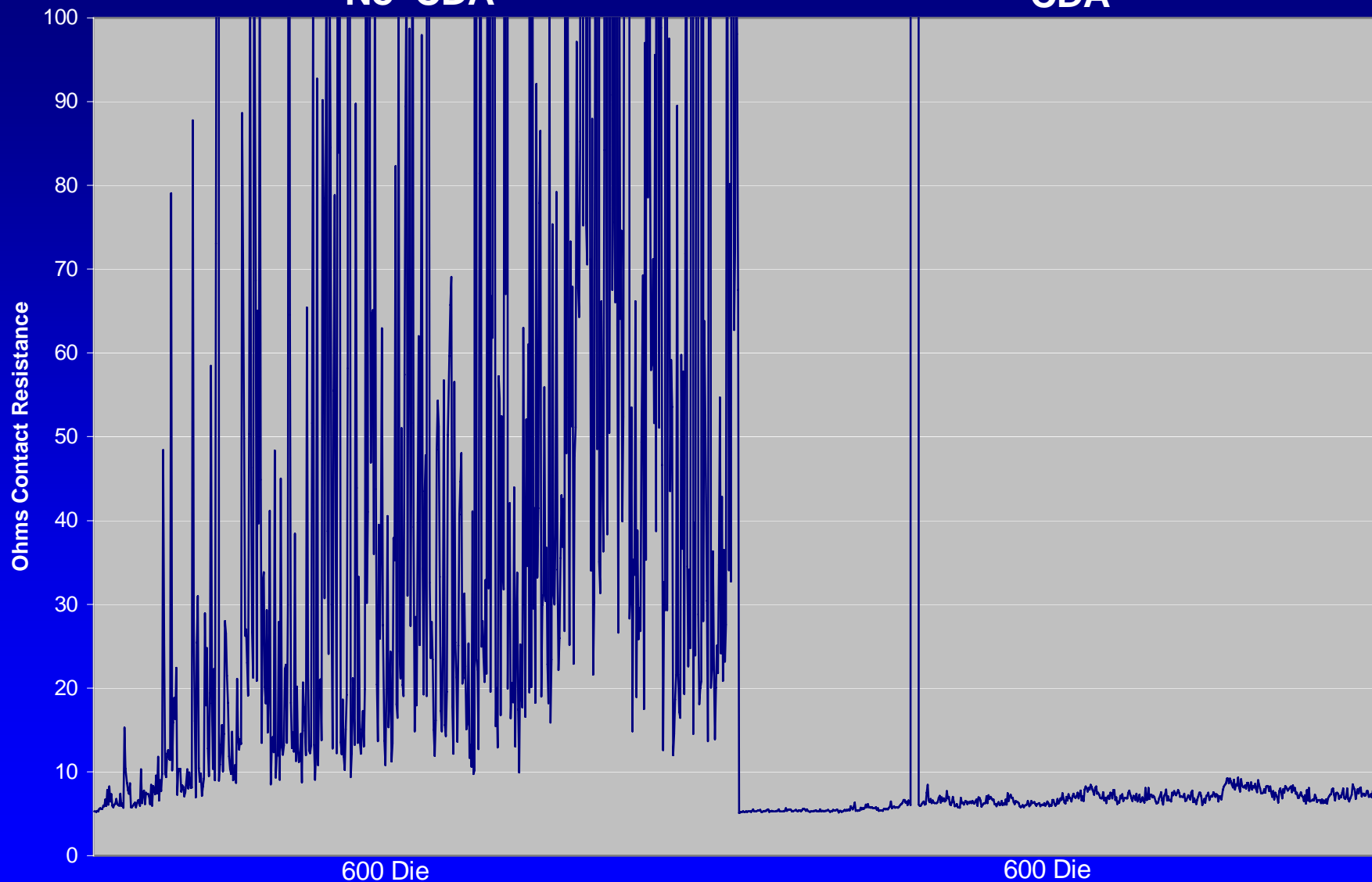
Single Power Pin Maximum Contact Resistance (MAXCRES)



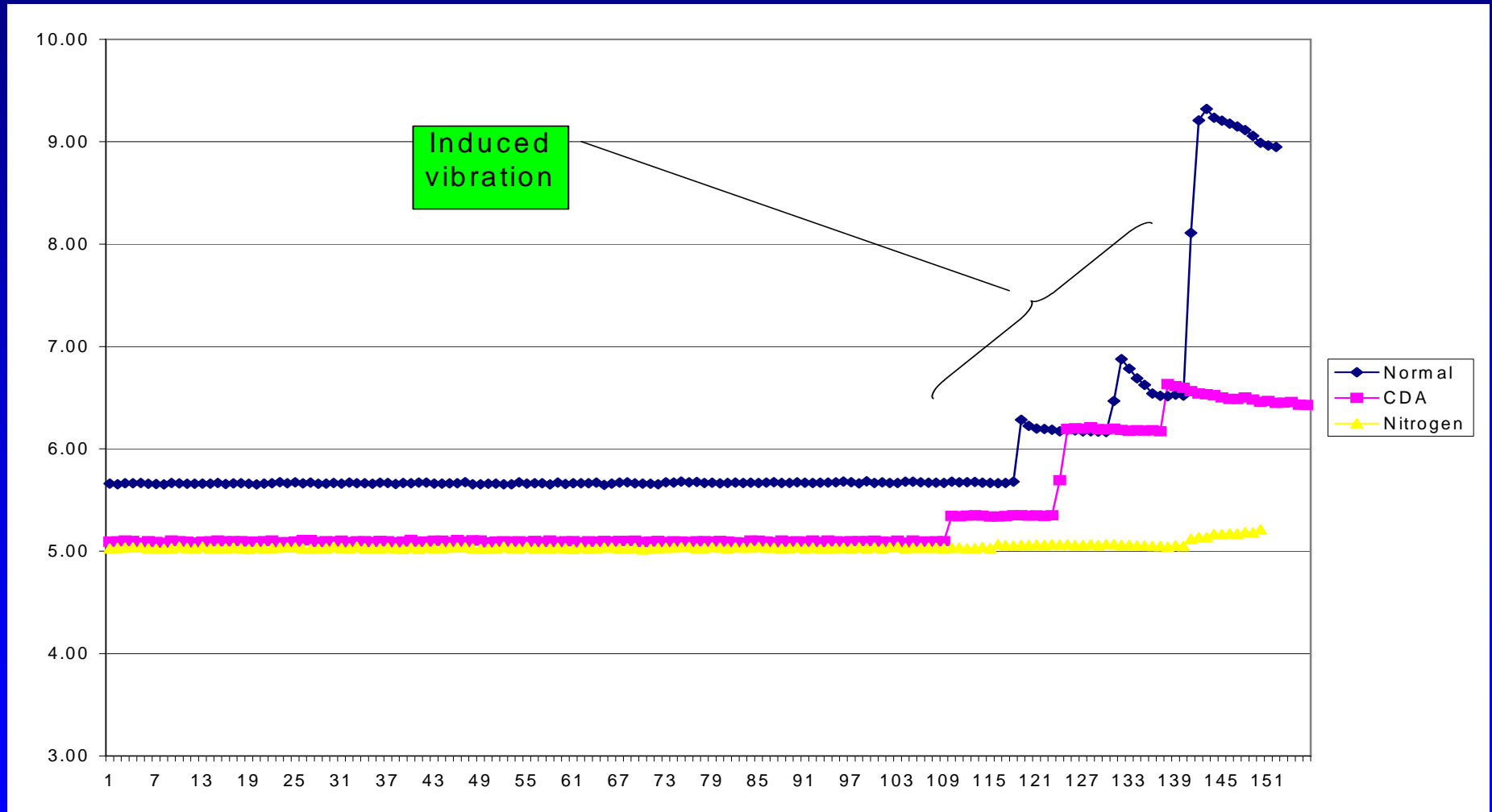
Max Contact Resistance wo/w CDA

No CDA

CDA



Effectiveness of CDA vs. Nitrogen Purge



Oxidation Theory

● Consider the Mechanical Contact to Al Pads

- A native oxide layer of Al_2O_3 exists on the Al pads to be tested at probe
- Some of this native oxide is removed by the mechanical probing & good contact is made by mechanical abrasion
- However, once micro-contacts are made, local heating can lead to oxide growth in the presence of air, leading to the formation of Al_2O_3 ($\Delta G^\circ \sim -400\text{kcal}$, therefore spontaneous)
- In the presence of moisture, hydrated aluminum oxides ($\text{Al}_2\text{O}_3 + \text{H}_2\text{O}$) are formed which can be thicker & more porous than the native Al_2O_3
- The hydrated oxides are colorless to white and can lead to resistive or semiconducting contacts¹

● CDA Purge Effects on Contact Process

- Elimination of moisture and therefore, hydration of the oxide

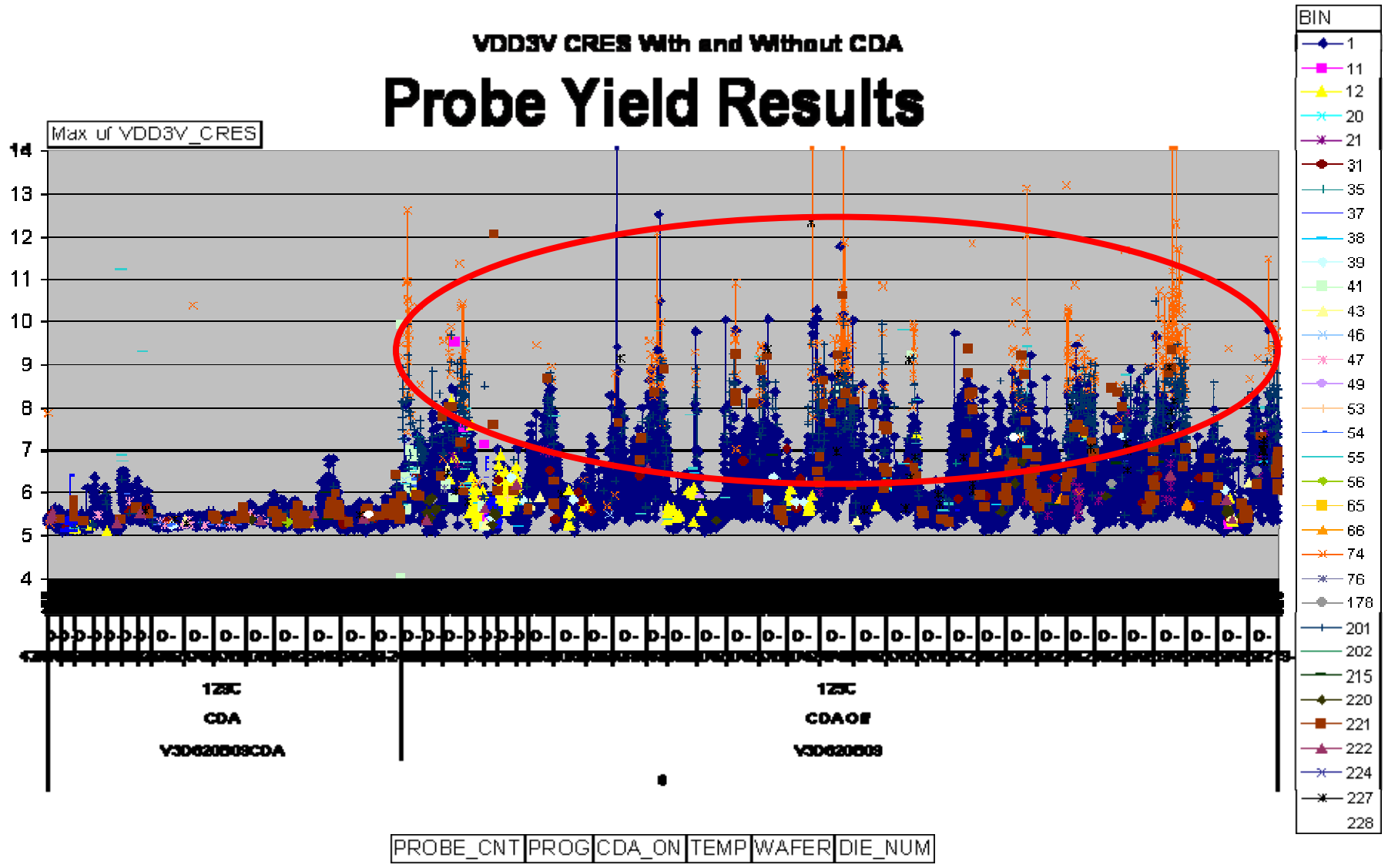
¹Broz & Rincon, "Probe Contact Resistance During Elevated Temperature Wafer Test," ITC Proceedings, p. 396, 1999.

CDA Contamination Within Factory Specs.

- Moisture readings pre and post filter (Spec ~ 100 ppm)
 - Pre filter was at 9.02 ppm after 14 hours of analysis
 - Post filter was at 10.8 ppm and dropping after only 2 hours of analysis
- Hydrocarbon (THC) readings from pre and post filter (Spec ~ 5 ppm)
 - Both Samples were analyzed using a GC/FID for total hydrocarbons (THC) as CH₄ per the site specification for CDA
 - The pre filter sample averaged 3.26 ppm THC as CH₄
 - The post filter sample averaged 3.46 ppm THC as CH₄

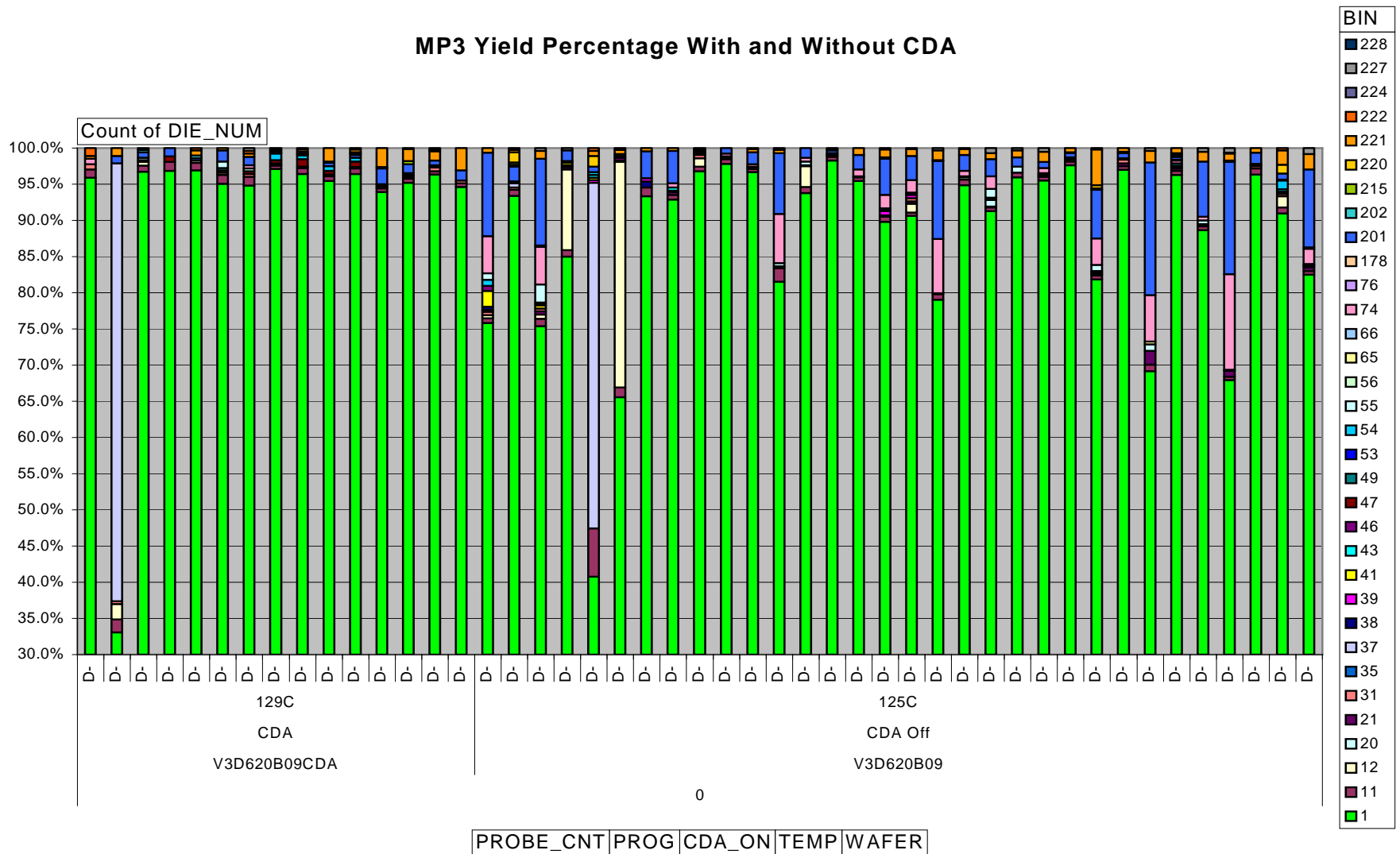
VDD3V CRES With and Without CDA

Probe Yield Results



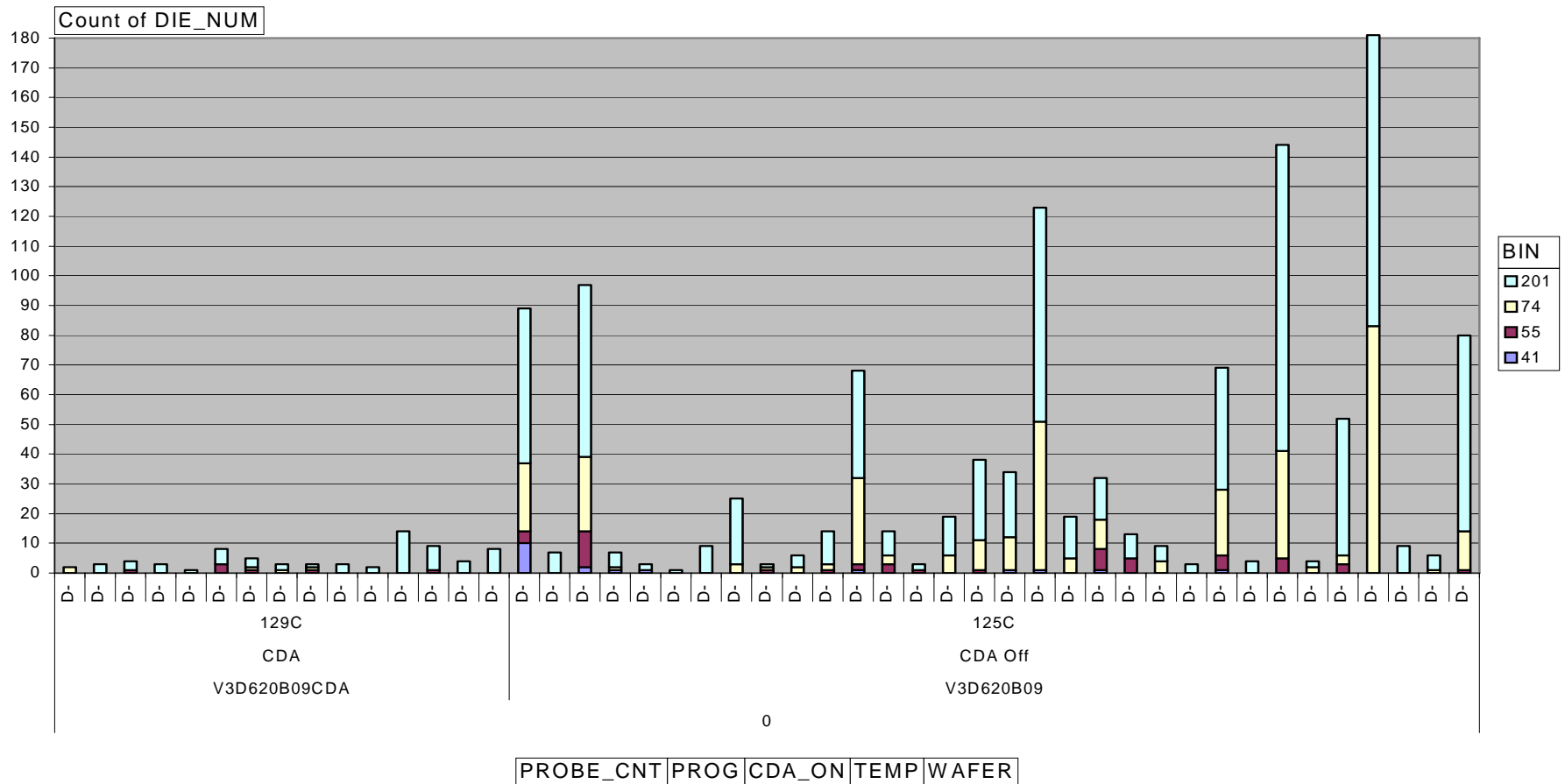
CDA vs. Non - CDA Results

MP3 Yield Percentage With and Without CDA



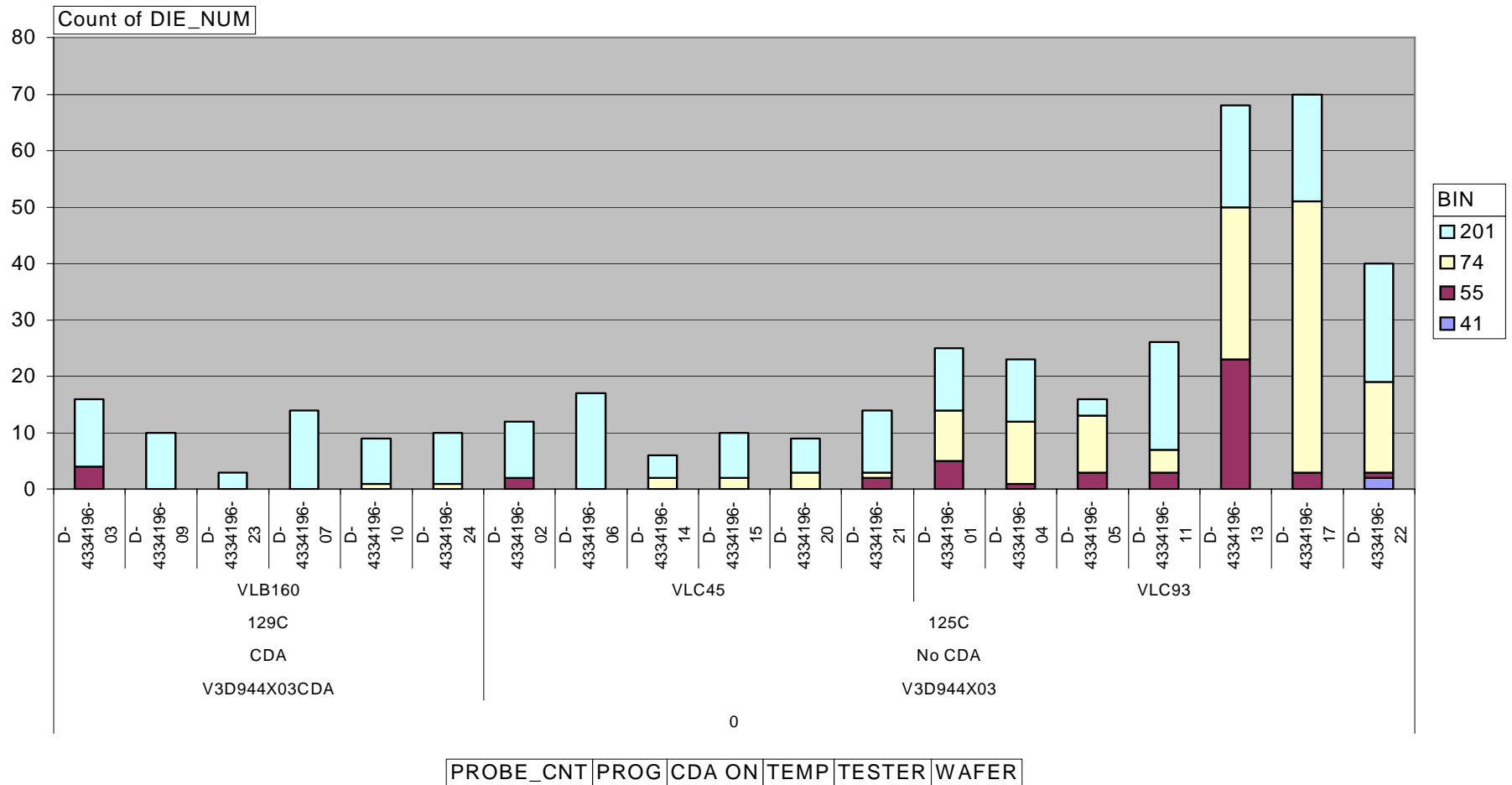
CDA vs. Non - CDA Results

Contact Sensitive Fallout (Bins 41, 55, 74, and 201) With and Without CDA



CDA vs. Non - CDA Results

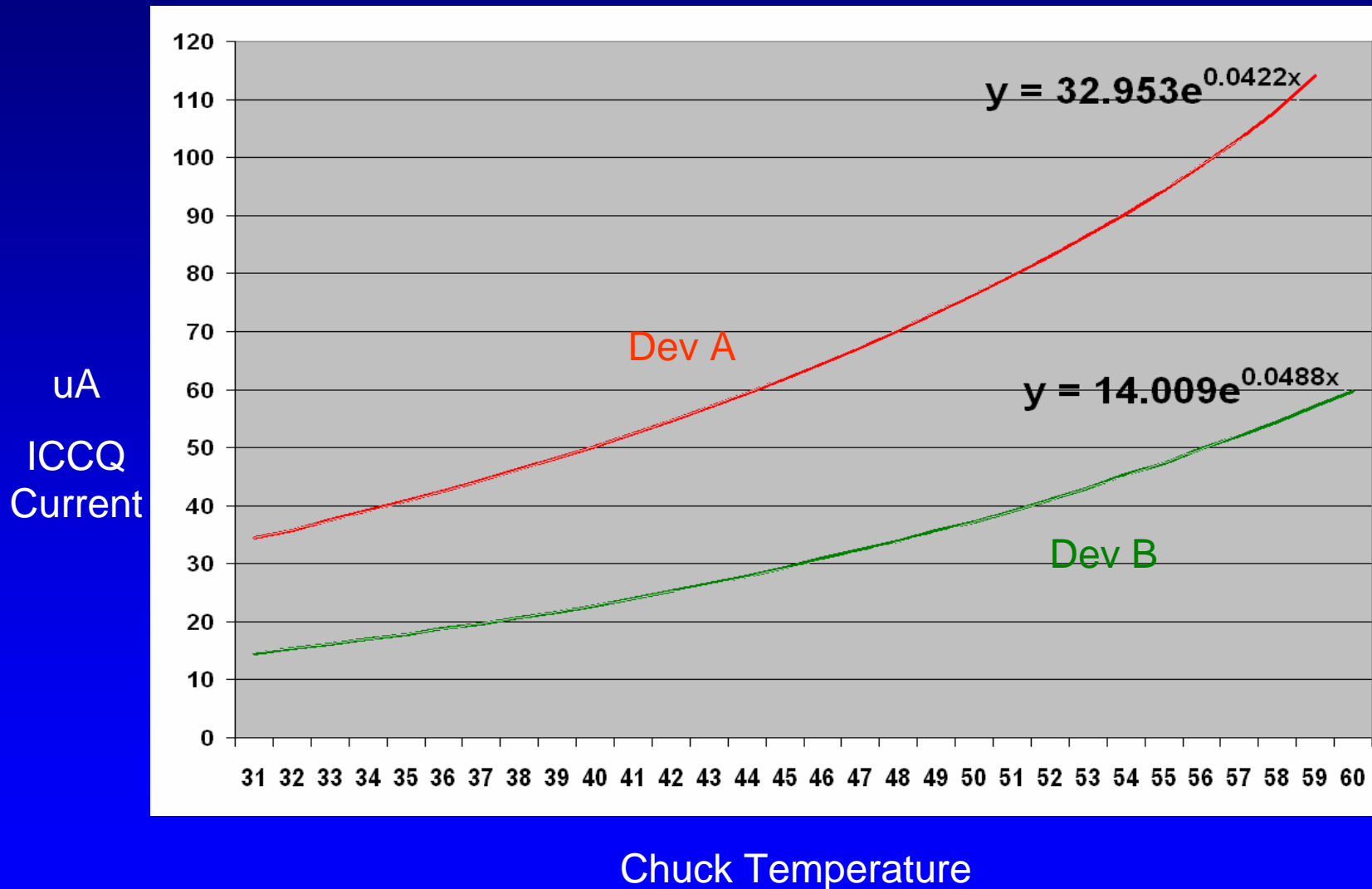
Contact Sensitive Fallout (Bins 41, 55, 74, and 201) With and Without CDA



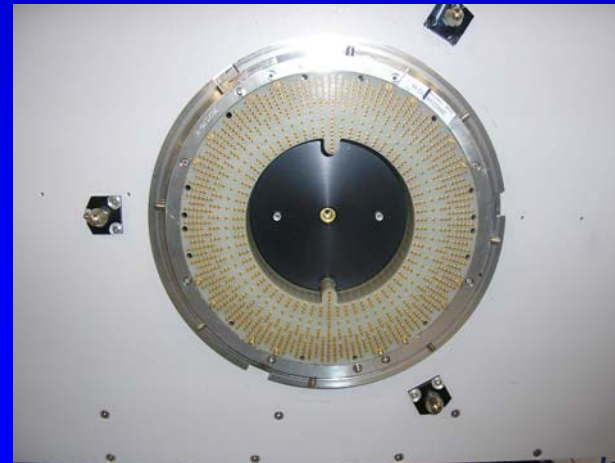
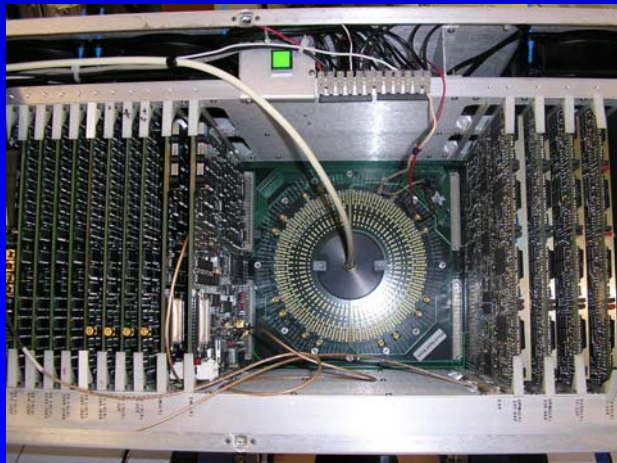
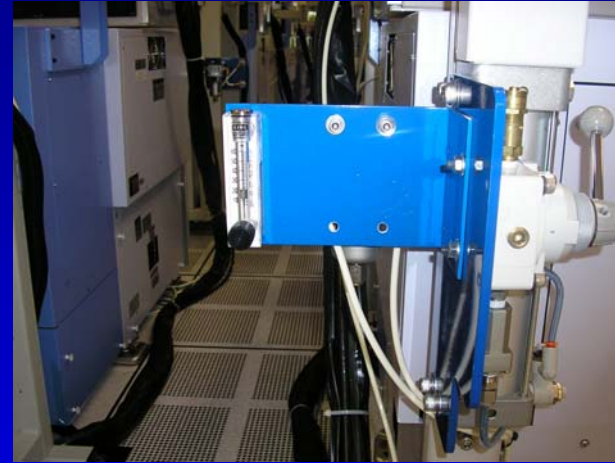
CDA influence on die temperature

- Response of ICCQ to chuck temperature was characterized with no CDA.
- CDA was injected at room temp (30°C) and hot chuck(125°C). Changes in ICCQ were recorded
- The equation $(\text{CDA Temp} - \text{Chuck Temp}) / 45^\circ\text{C}$ closely defines the effect of CDA on die temperature.
 - CDA temperature is 20°C typical
 - Die temp is effected by $<1^\circ\text{C}$ at 30°C chuck temperature
 - Die temp is effected by 2-4°C at 125°C chuck temperature

Effect of chuck temperature on ICCQ current



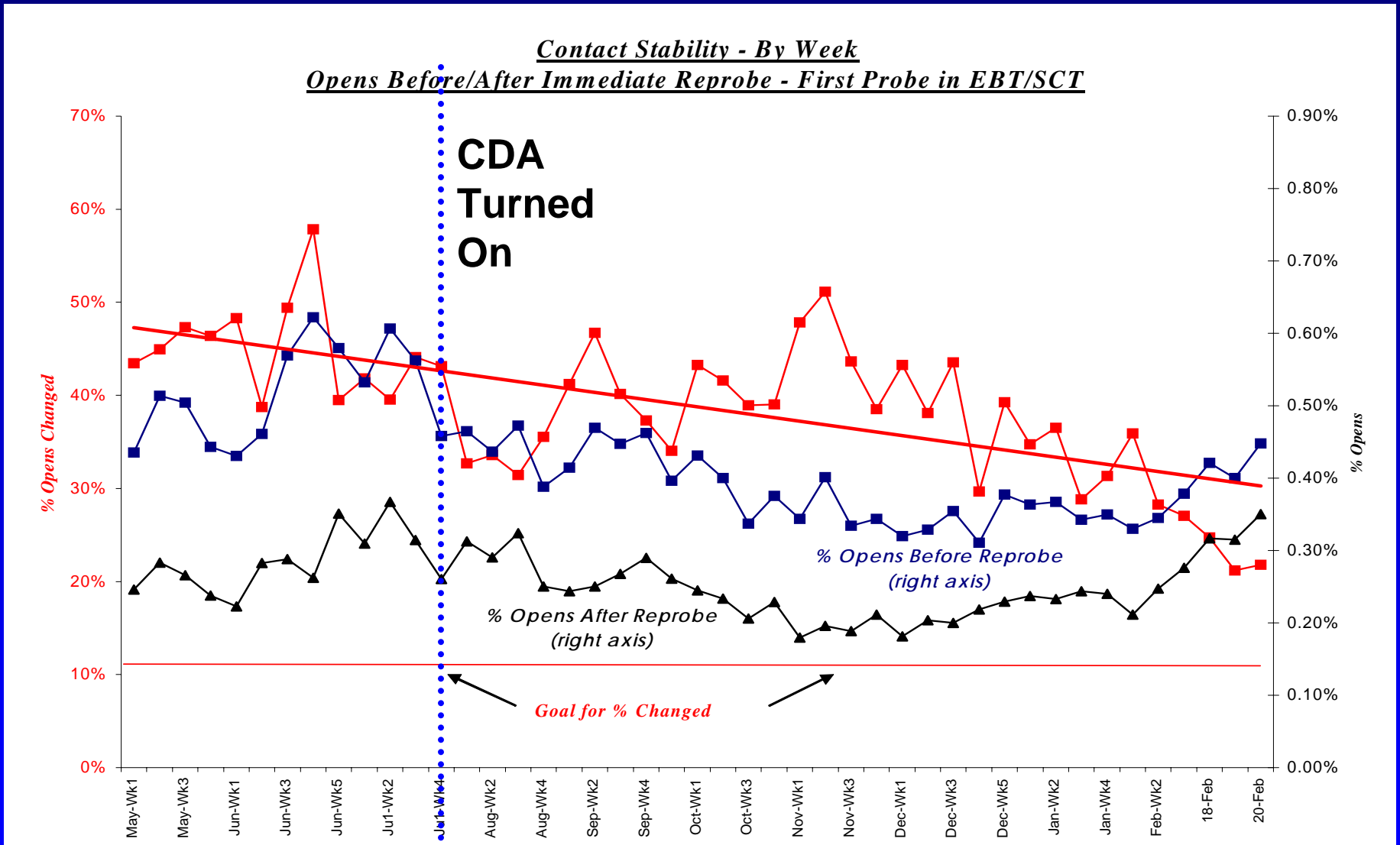
CDA Hardware Example



No Measurable ESD Buildup

- Measured ESD on probe needles
 - ACL Model 300B Electrostatic Locator
 - Two testers
 - CDA on needles
 - Measure every 15 minutes
 - No Measurable static build up <1v

Impact on First Pass Opens



Conclusion

- An in-situ method of stabilizing contact resistance using CDA (compressed dry air)
- Reducing oxidation and contaminate build up
- Maximizing yield and reducing reprobe on contact sensitive BINs
- Reduces the need to increase cleaning intervals. This results in longer probe card life and improved throughput.

Acknowledgements

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Thanks For Listening –
Enjoy the Conference