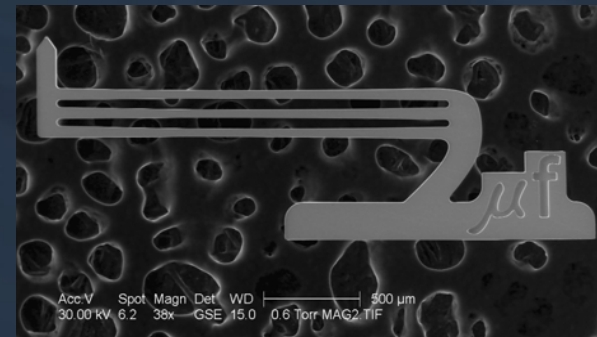


Mechanical Design of MEMS Probes for Wafer Test

Chris Folk



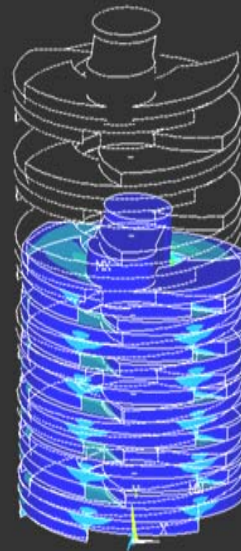
Outline

- Microfabrica's EFAB[®] process
- EFAB process applied to Compliant Pins
- Design of a Compliant Pin
- EFAB process applied to a Vertical MEMS probe
- Design of Vertical MEMS probe
- Conclusions

EFAB[®] Technology Summary

- Multi-layer metal manufacturing technology for micro- to millimeter-scale devices
- Unlimited variety of complex 3-D shapes can be built
 - Designers are not constrained to standard shapes and processes
- Micron-precision features
 - Tolerances ~ 2 micron typical
- Utilizes wafer-scale batch process

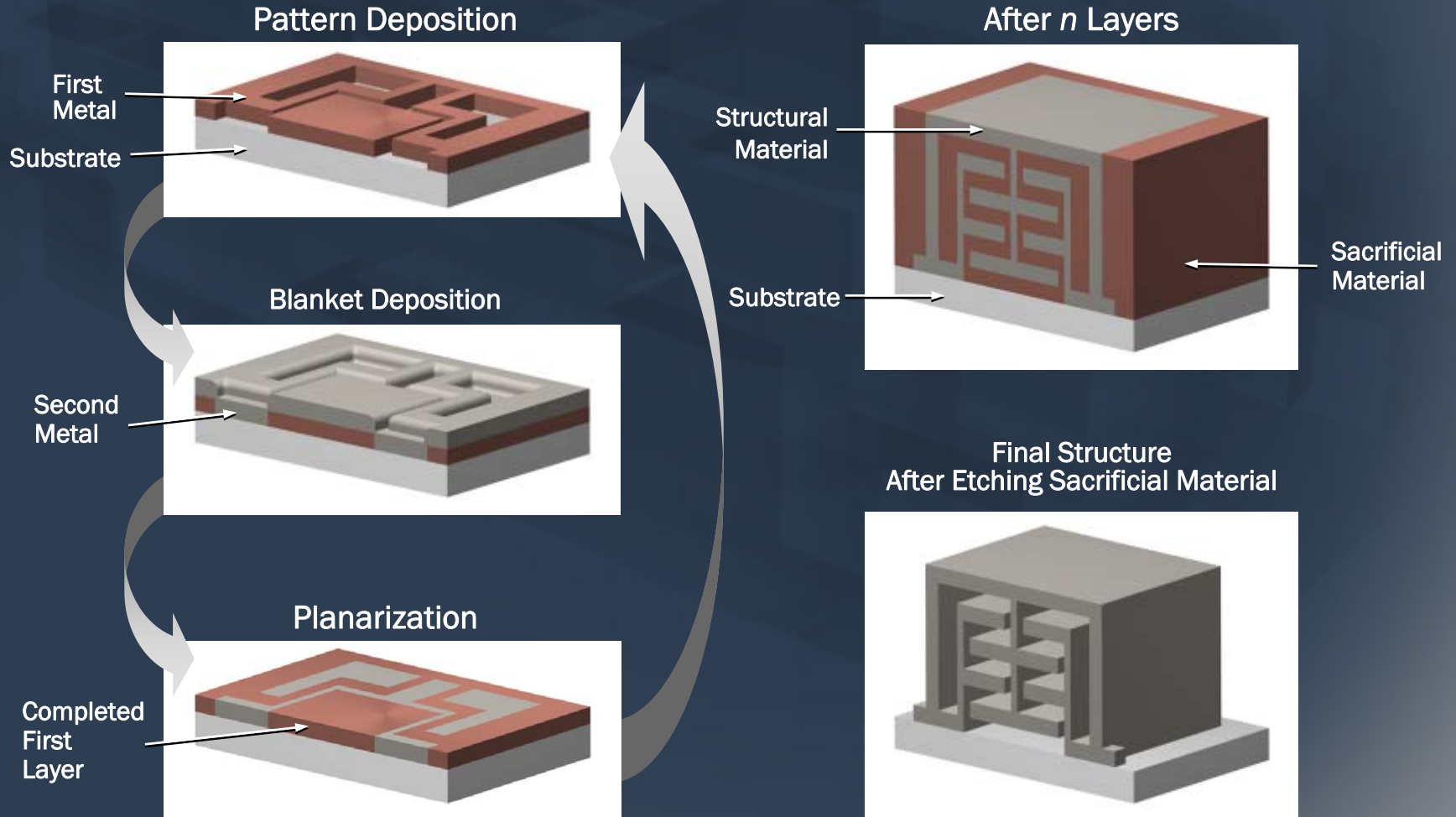
From 3-D CAD
Design and
Simulations



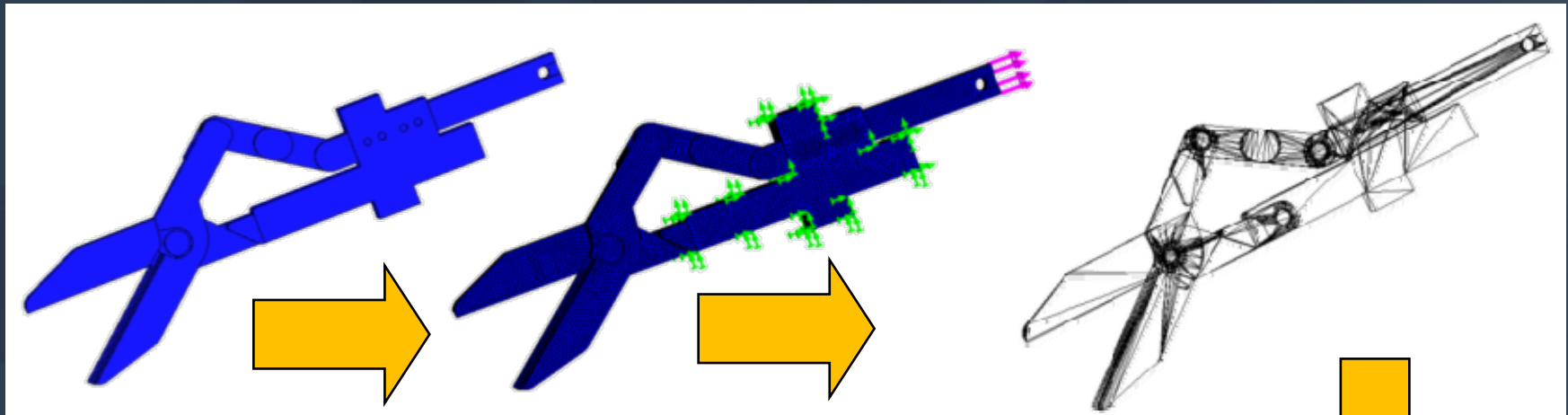
to Microdevice



EFAB Process Flow



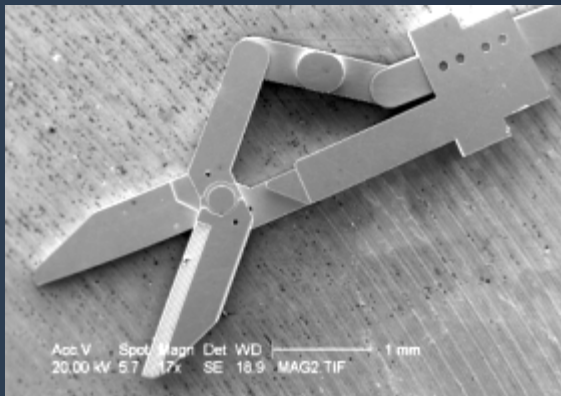
EFAB Design Flow



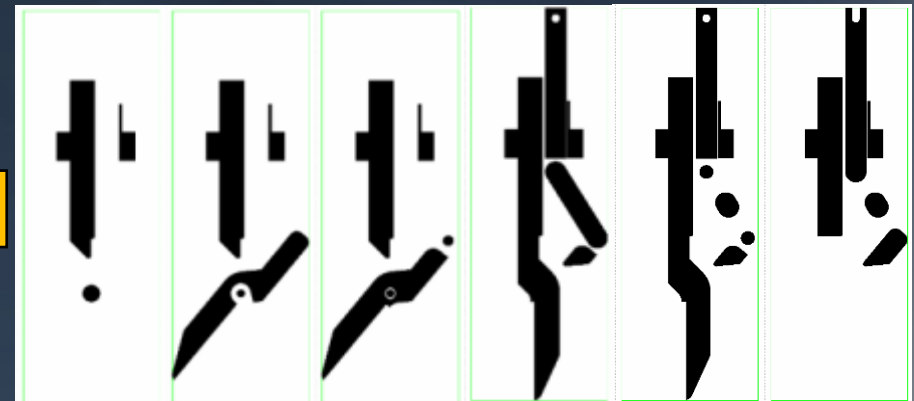
Solid Model

Simulation

STL File Export



Fabricated Device

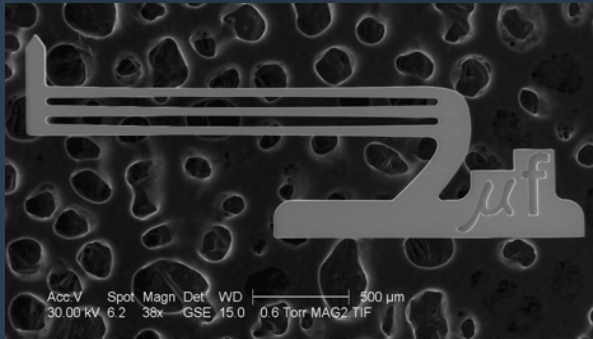


LayerView™ Cross-sectioning

Advantages of EFAB Technology for Wafer Probes

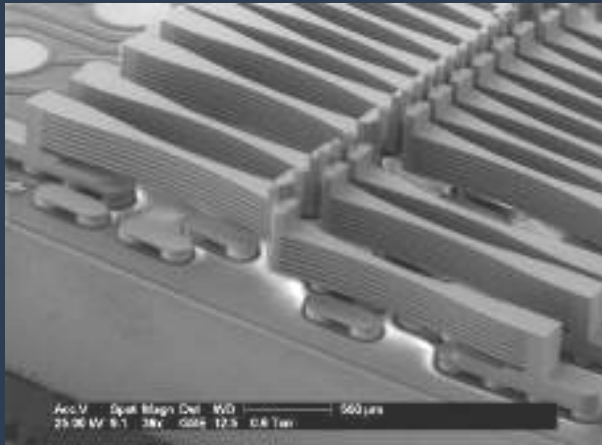
- Lithography-based batch manufacturing
 - Precise and very uniform pin dimensions
 - Arbitrary complex geometries = design flexibility
- Two-metal structure for optimum performance
 - Nickel-cobalt alloy Valloy™-120 body for best spring behavior
 - Rhodium-based Edura™-180 tips for low wear & excellent contact resistance

Wafer Probe Products Using EFAB



Compliant Pins

- Custom-made precision individual springs and spring pins for wafer probing and fine-pitch socket applications

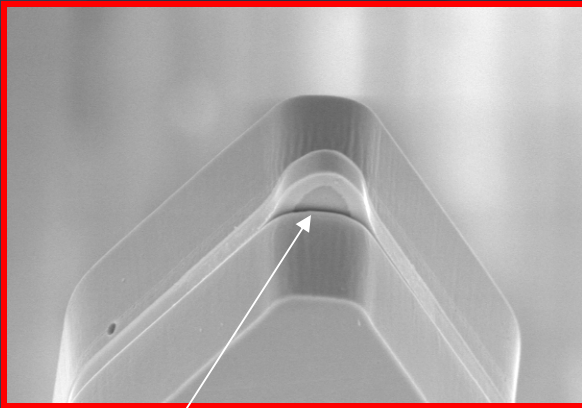


Vertical MEMS (VMEMS) Probes

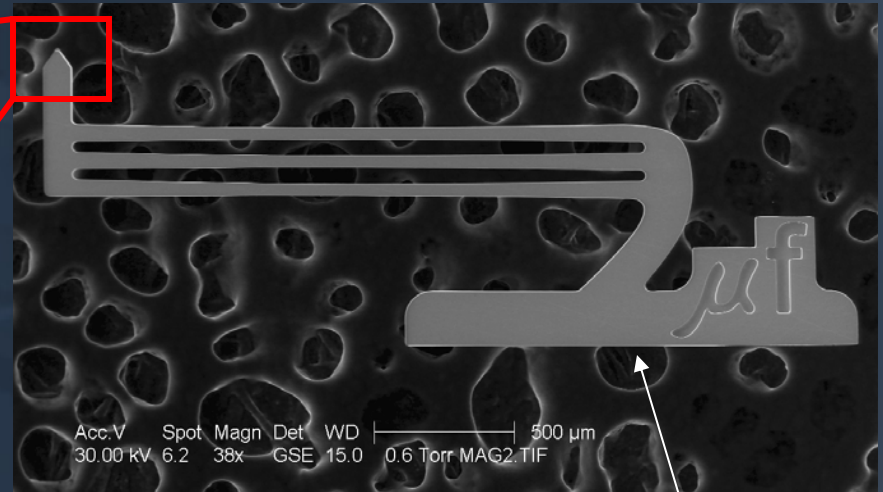
- Cantilevered structures for memory test
- 50 μm pad pitch demonstrated
- Enables high parallelism multi-site applications

Compliant Pins

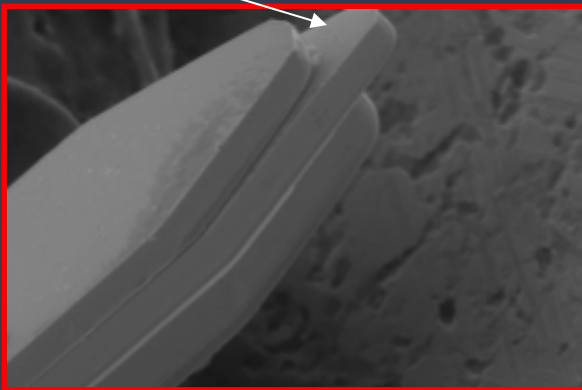
- Different probe styles (cantilever, buckling beam) and arbitrary tip shape can be designed to meet desired specifications.



Edura™-180 rhodium based tip



Valloy™- 120 proprietary nickel-cobalt alloy



How to Design a Compliant Pin

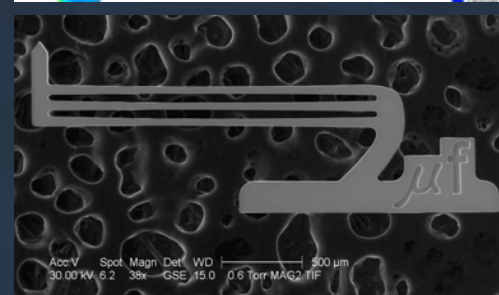
- Review prober and probe card requirements
- Determine range of probe card flexure, probe tip planarity
- Determine force and scrub. When designing pins with EFAB, force and scrub are decoupled. Therefore, good Cres is achieved by tuning these parameters.
- Usable overtravel for an individual pin is determined by:
 - first pin: minimize fatigue, creep, pad damage
 - last pin: have sufficient force and scrub to achieve good Cres
- Testing validates choices, or back to the drawing board!



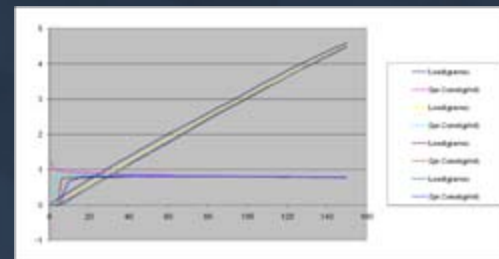
CAD



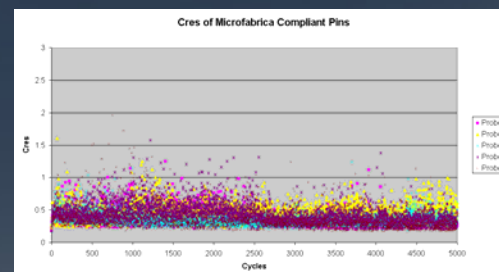
FEA



Fabricate



Mechanical test



Electrical test

Simple Cantilever

For a point load applied at the end of a beam:

Maximum deflection

$$d = PL^3 / (3EI)$$

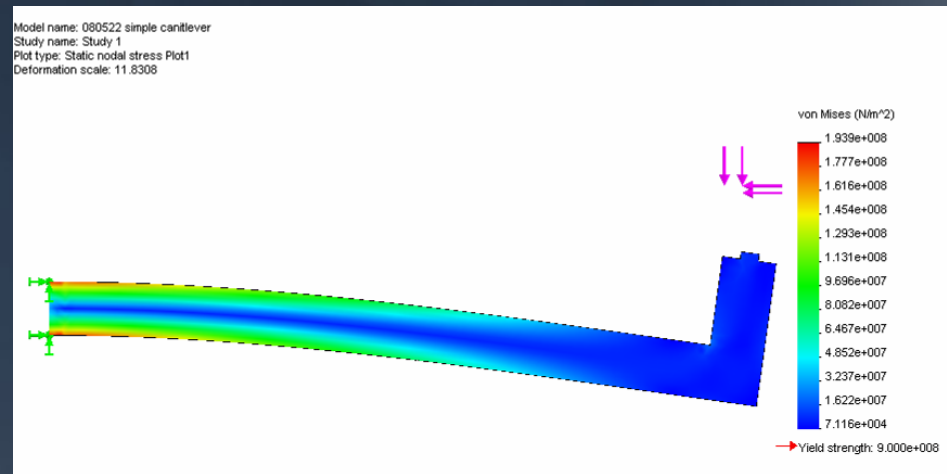
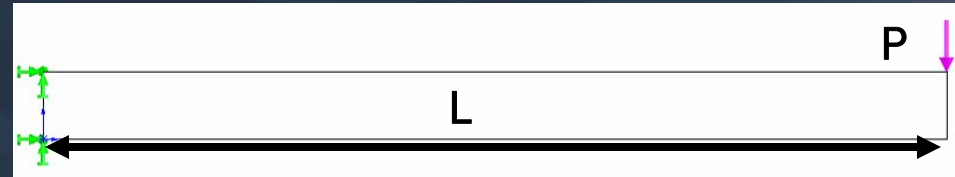
Equation of elastic curve

$$y = P(x^3 - 3Lx^2) / 6EI$$

I = moment of inertia

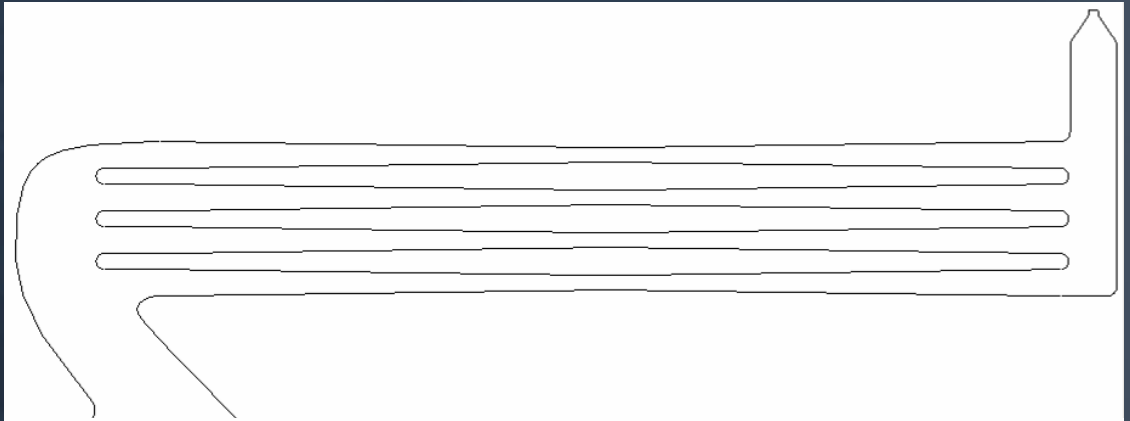
Add friction and probe neck

Stress concentrated at root of cantilever. Probe scrub coupled to stiffness of probe.

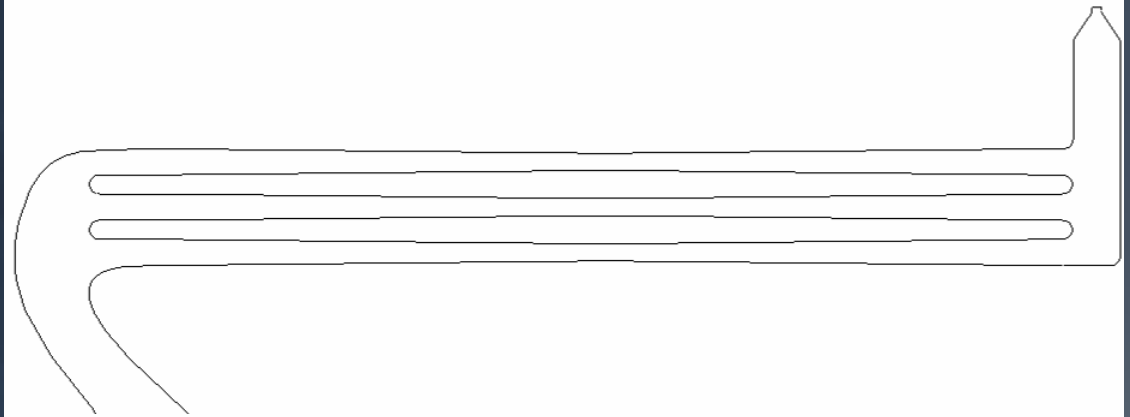


Why multi-beam cantilevers?

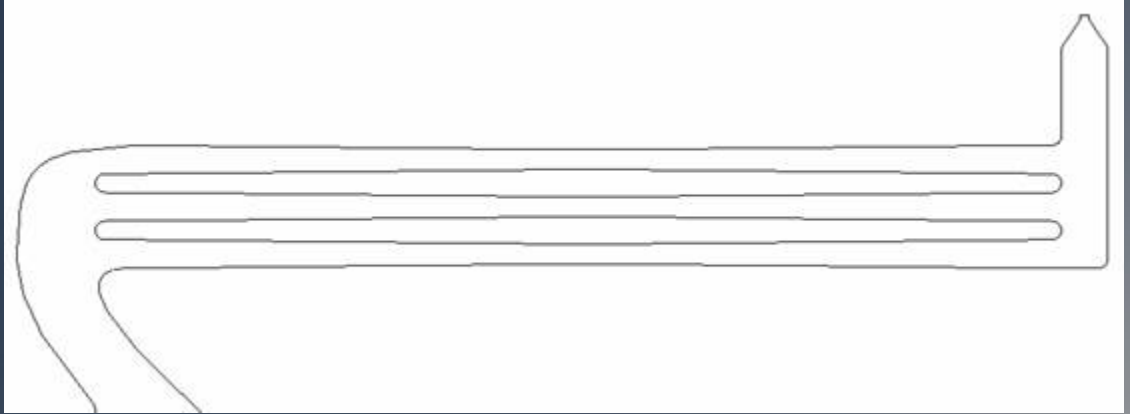
Short scrub, 0.75 g/mil



Long scrub, 0.5 g/mil

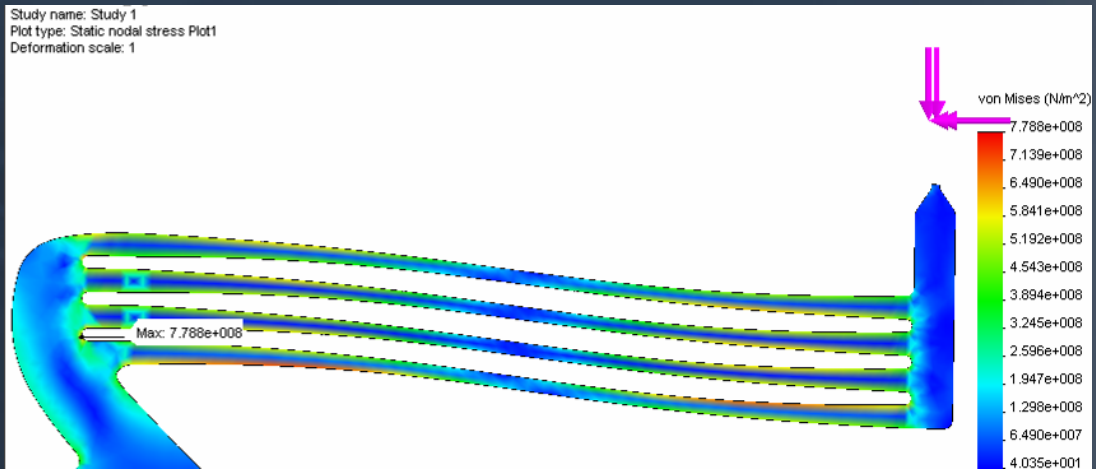


Long scrub, 0.75 g/mil

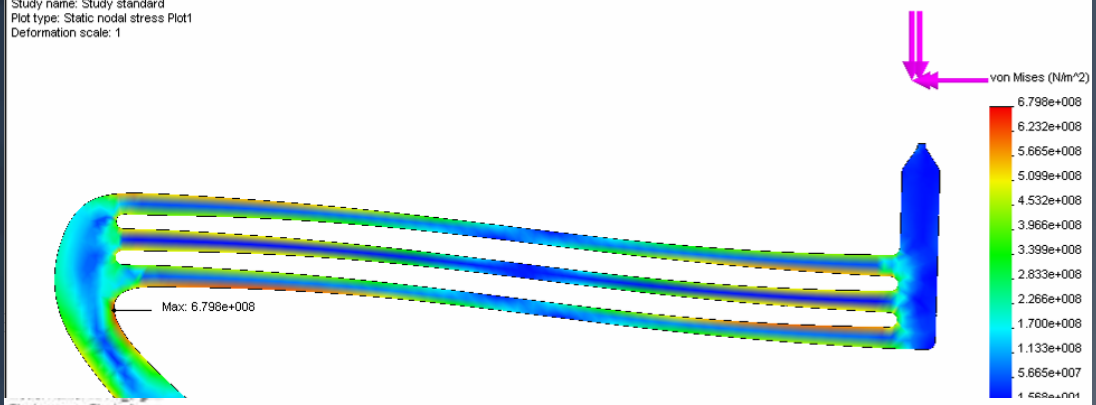


FEA used to determine Von Mises stress

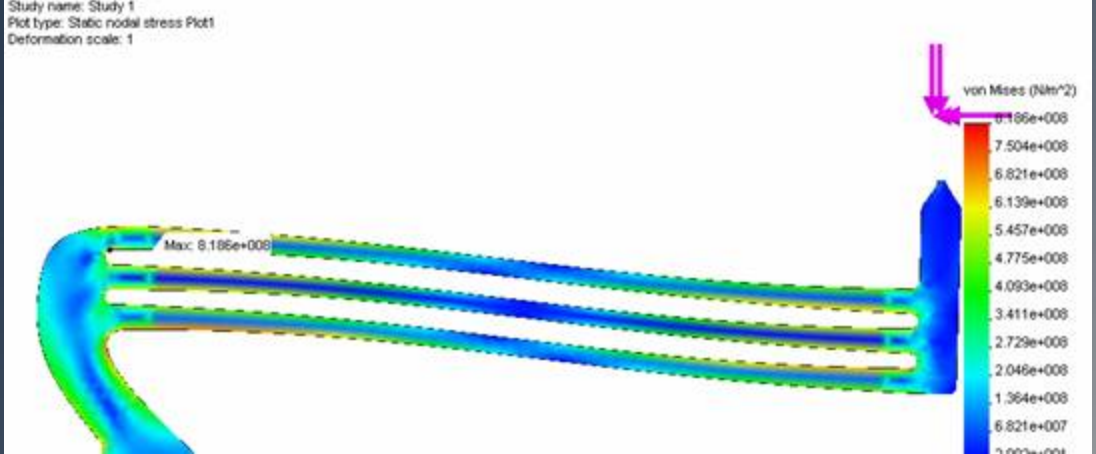
Short scrub, 0.75 g/mil



Long scrub, 0.5 g/mil



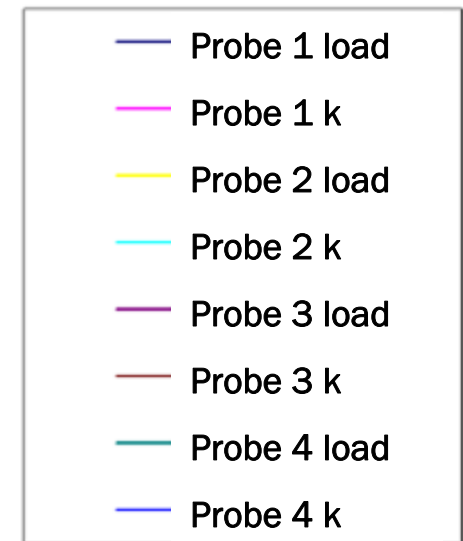
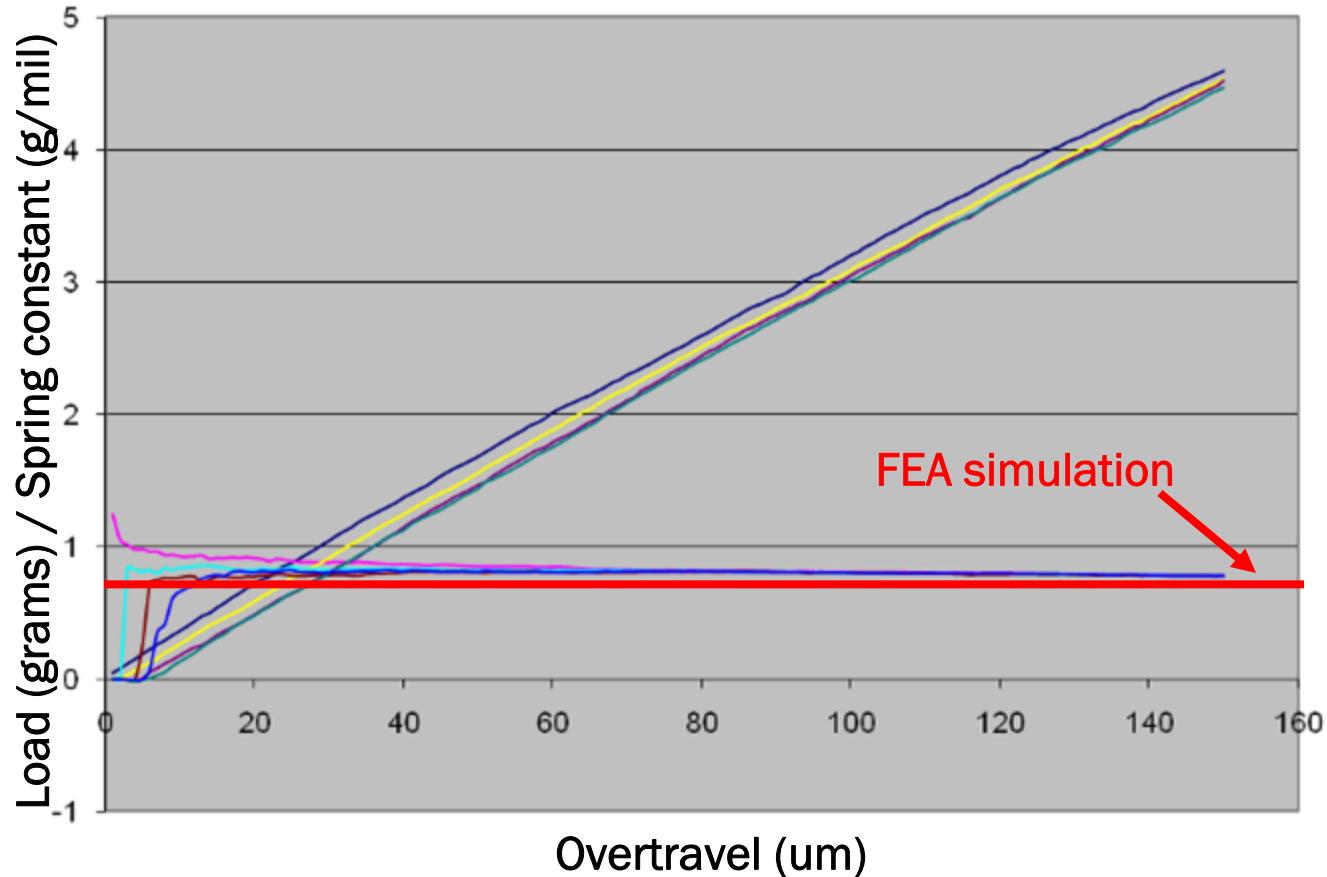
Long scrub, 0.75 g/mil



Design Tradeoffs Impact Pin Performance

Probe Name	Short scrub, 0.75 g/mil	Long scrub, 0.5 g/mil	Long scrub, 0.75 g/mil
Computed spring constant	0.75 g/mil	0.5 g/mil	0.75 g/mil
FEA Applied force (g)	5.00	3.30	5.00
Computed overtravel (um)	167	170	168
Computed scrub motion (um)	8	16	16
Max Von Mises σ (MPa)	780	680	820
OT required for 2g force (um)	68	101	68
σ VM required for 2g force (MPa)	310	400	330

Spring Constant Matches Simulation



Cres Testing

0.75g/mil, long scrub probe

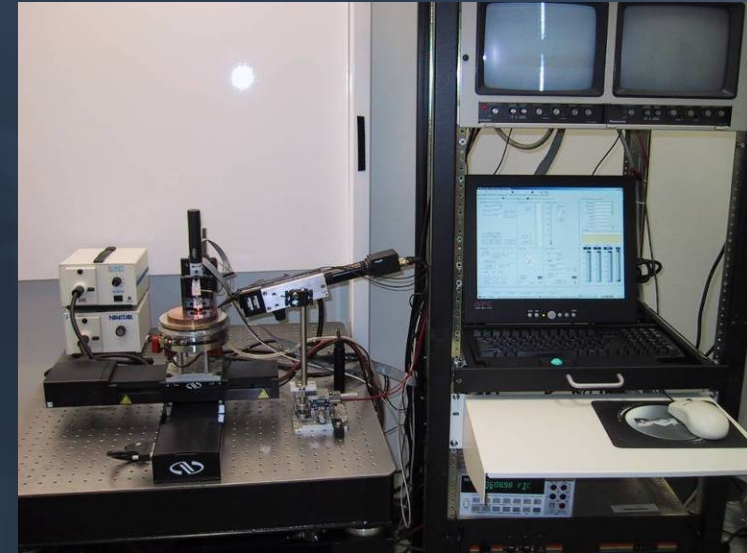
100 μm over travel

100°C

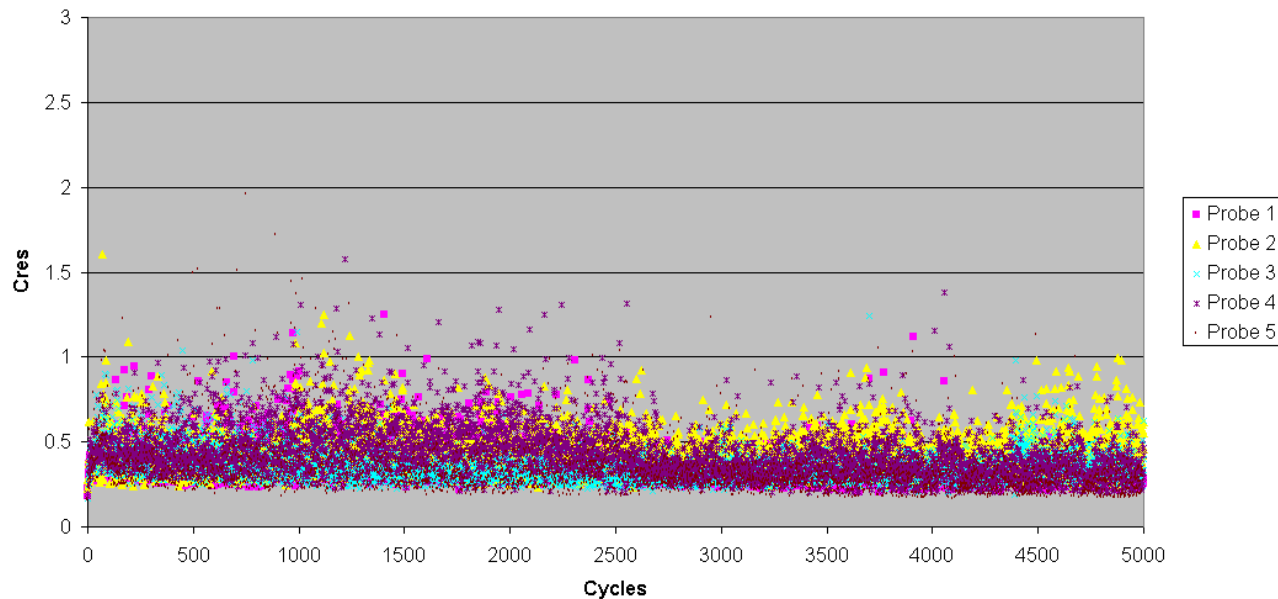
5000 cycles

Al on Si wafer

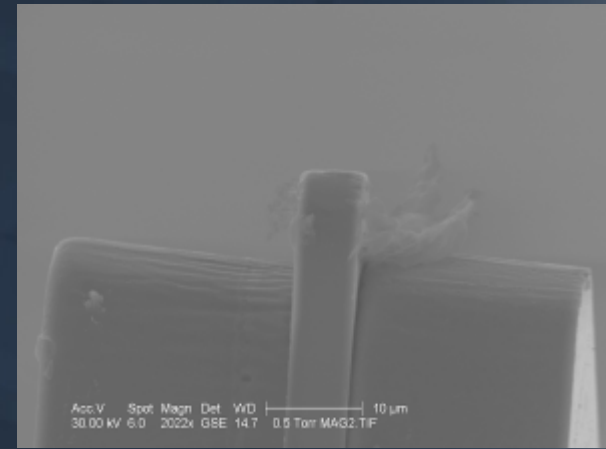
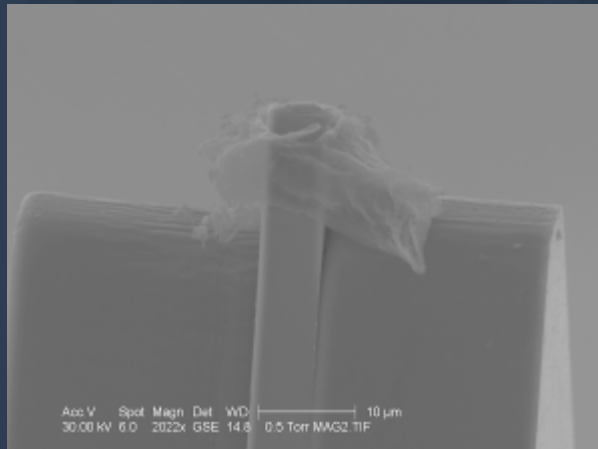
Without cleaning



Cres of Microfabrica Compliant Pins



Minimal Debris 5K – No Clean

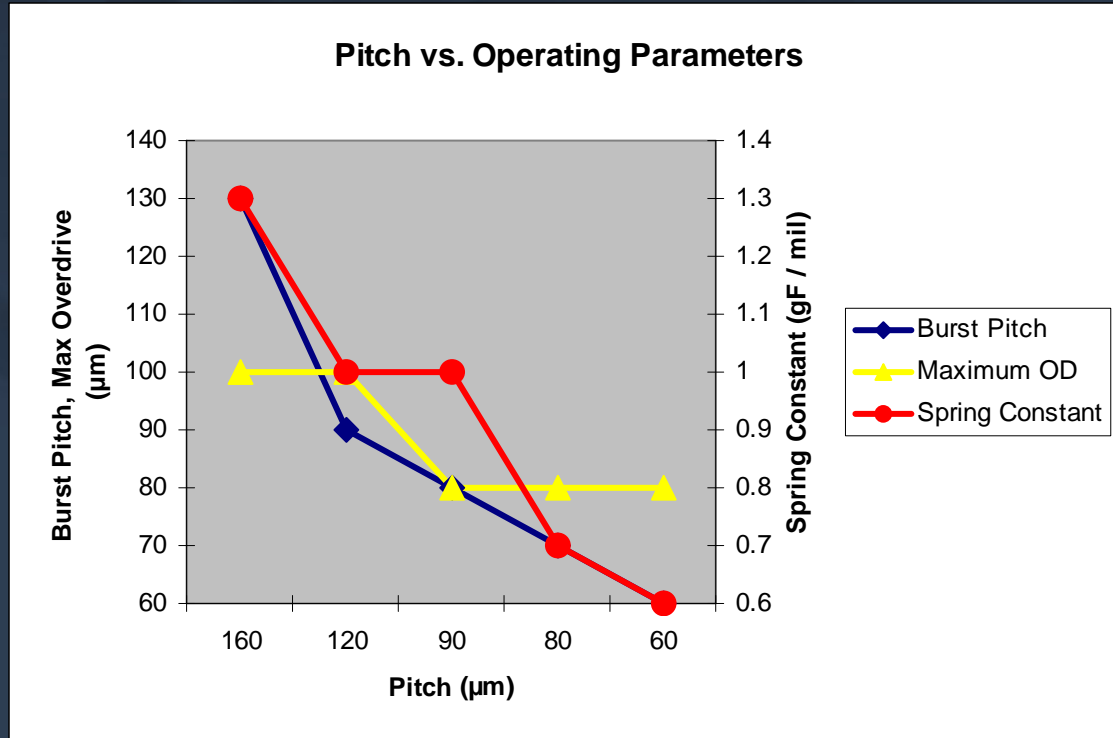


Vertical MEMS (VMEMS) Probes

- Custom-designed to meet specific force, compliance, height, footprint and scrub requirements
- Extremely tight linear pad pitches are possible

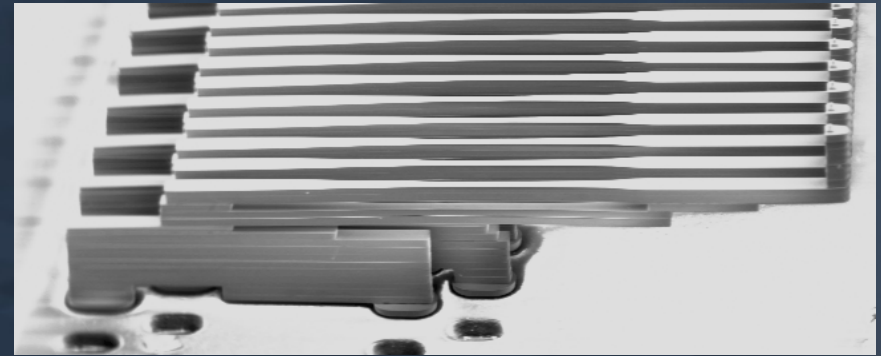


Pitch & Performance Tradeoffs

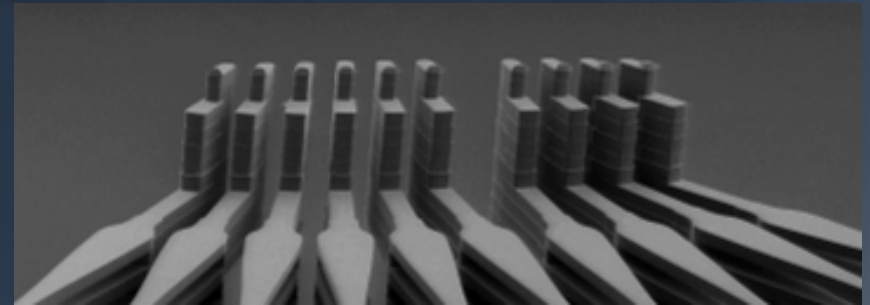
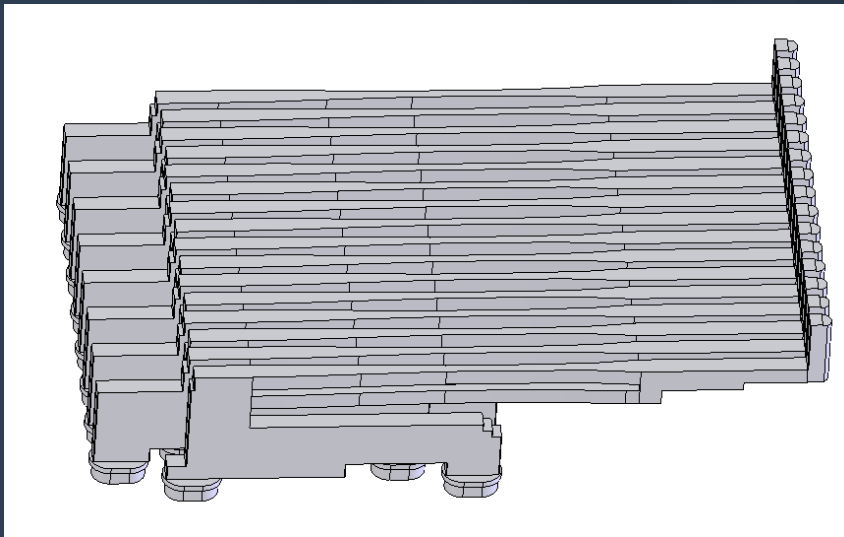


MF900 – 90 μm pitch

- Pitch:
 - True – 90 μm
 - Burst – 80 μm
- Over Drive: 80 μm
- Spring Constant: 1.0 g/mil



True

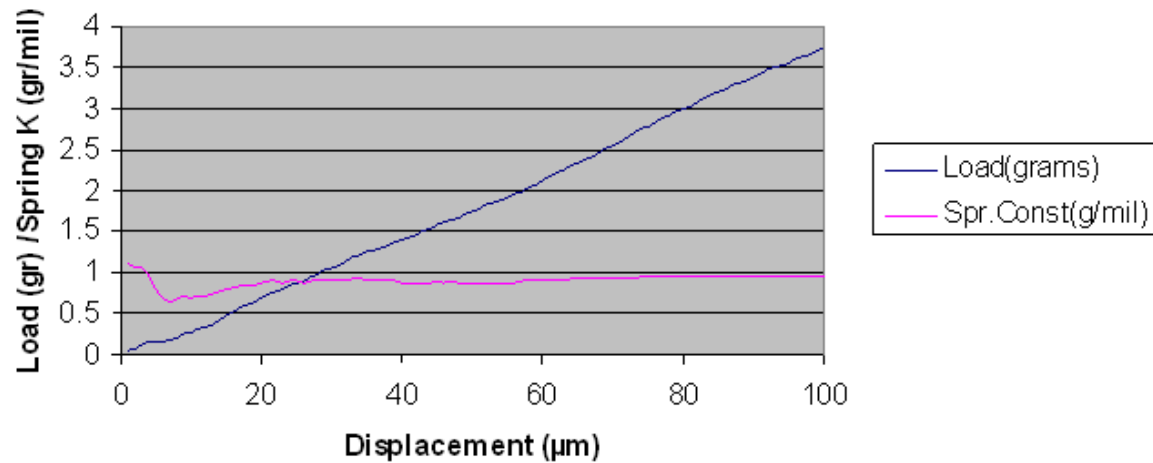


Burst

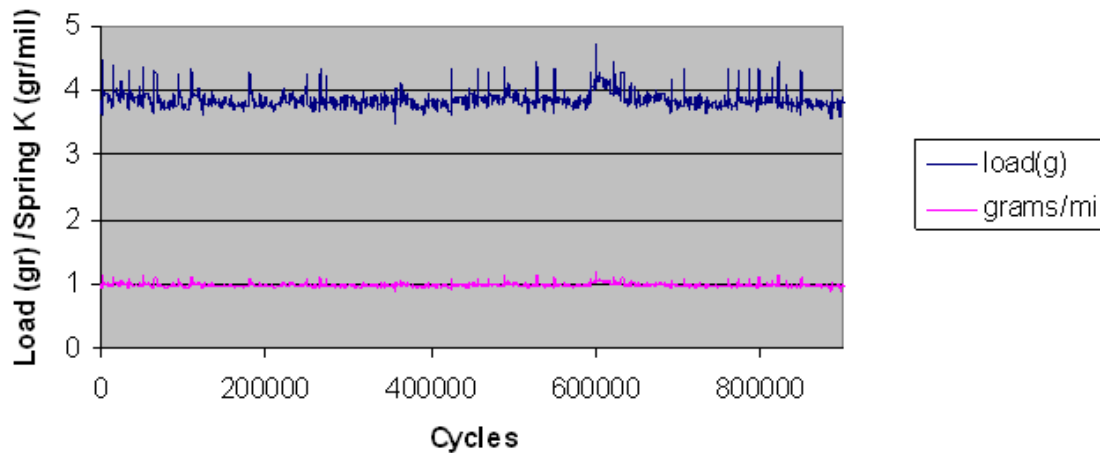
Mechanical Testing

- Designed spring constant = 1 gF/mil

Load vs Deflection of MF900 probe @ 100°C



MF900 cyclic test @ 100μm OT, 100°C



- Maintains consistent load >900k cycles

Conclusions

- EFAB process enables unique designs for building both Compliant Pins and VMEMS probes
 - Valloy™-120 high performance spring material
 - Edura™-180 excellent tip contact material
- Multi-beam cantilevers allow spring constant and scrub to be decoupled
- Well characterized materials and process enables closed loop of design -> simulation -> fabrication -> test
 - Measured performance of pins closely matches FEA
 - Sub-ohm Cres achieved
 - Tip design yields minimal debris