



SW Test Workshop

Semiconductor Wafer Test Workshop

June 7 - 10, 2015 | San Diego, California

Probe Pin Wideband Electrical Circuit Model



Mohamed Eldessouki
SV TCL – An SV Probe Company

Overview

- Motivation and Objective
- Introduction
- Closed Form Circuit Model
- Probe Pin Measurements and Simulation
- Probe Pin Modeling and Verification
- Summary and Conclusion

Motivation & Objective

Motivation

Customers are looking for Probe Head (PH) circuit model to be able to:

Simulate and Predict Bandwidth (BW)

Simulate and Predict Power Plane Input Impedance

Reduce risk probe hardware not to meet test expectations

Objective

Develop Close Form Accurate Circuit Model

Verify Developed Model Using:

Measured S-parameters

Ansoft HFSS Simulation Tool (Field Analysis)

Introduction

Trio Probe & Spring Pin

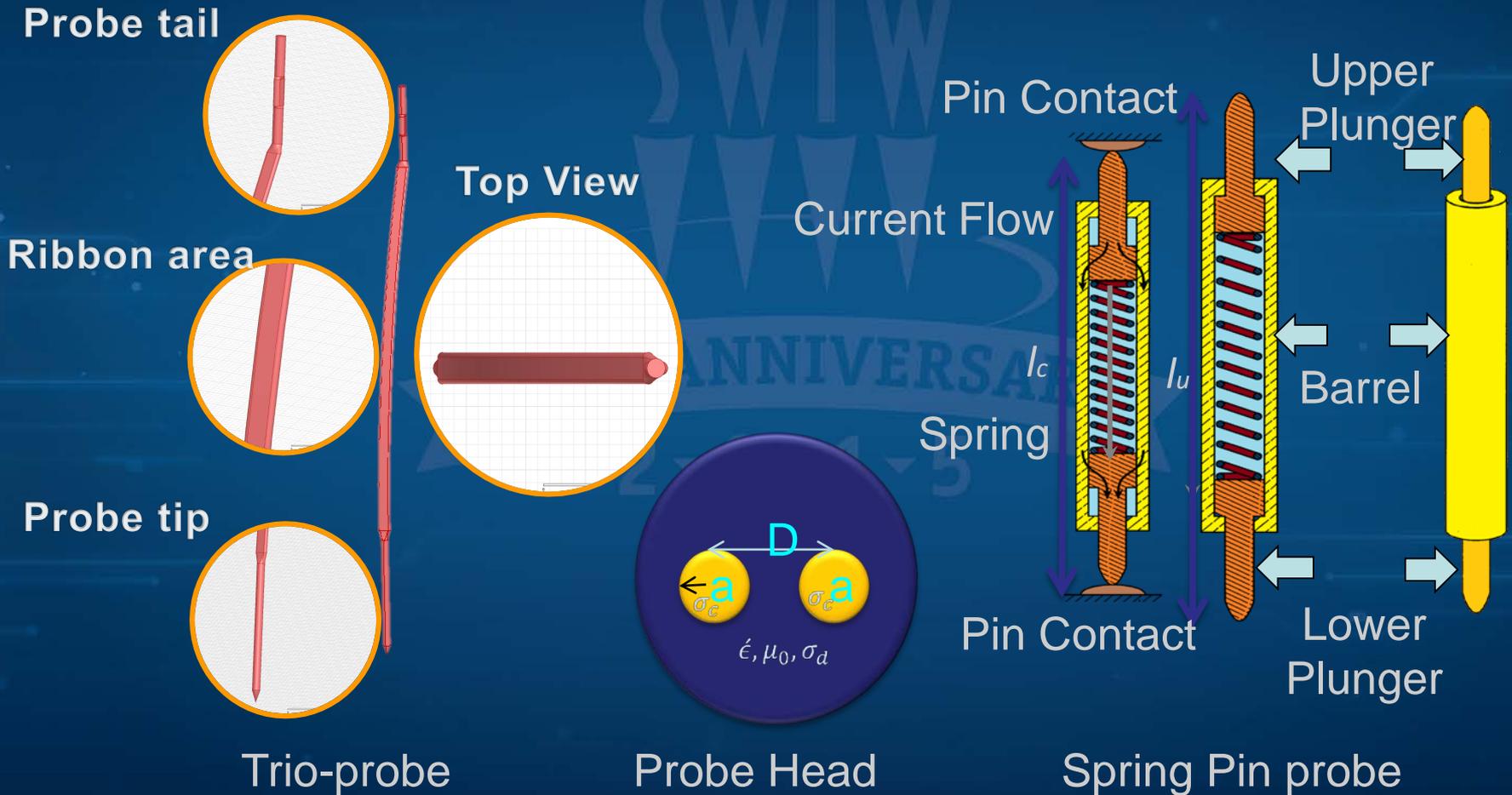
Proximity and Skin Effect

Circuit Model Comparison

Transmission Line (TL) Model

Introduction

Probe Pin Structure

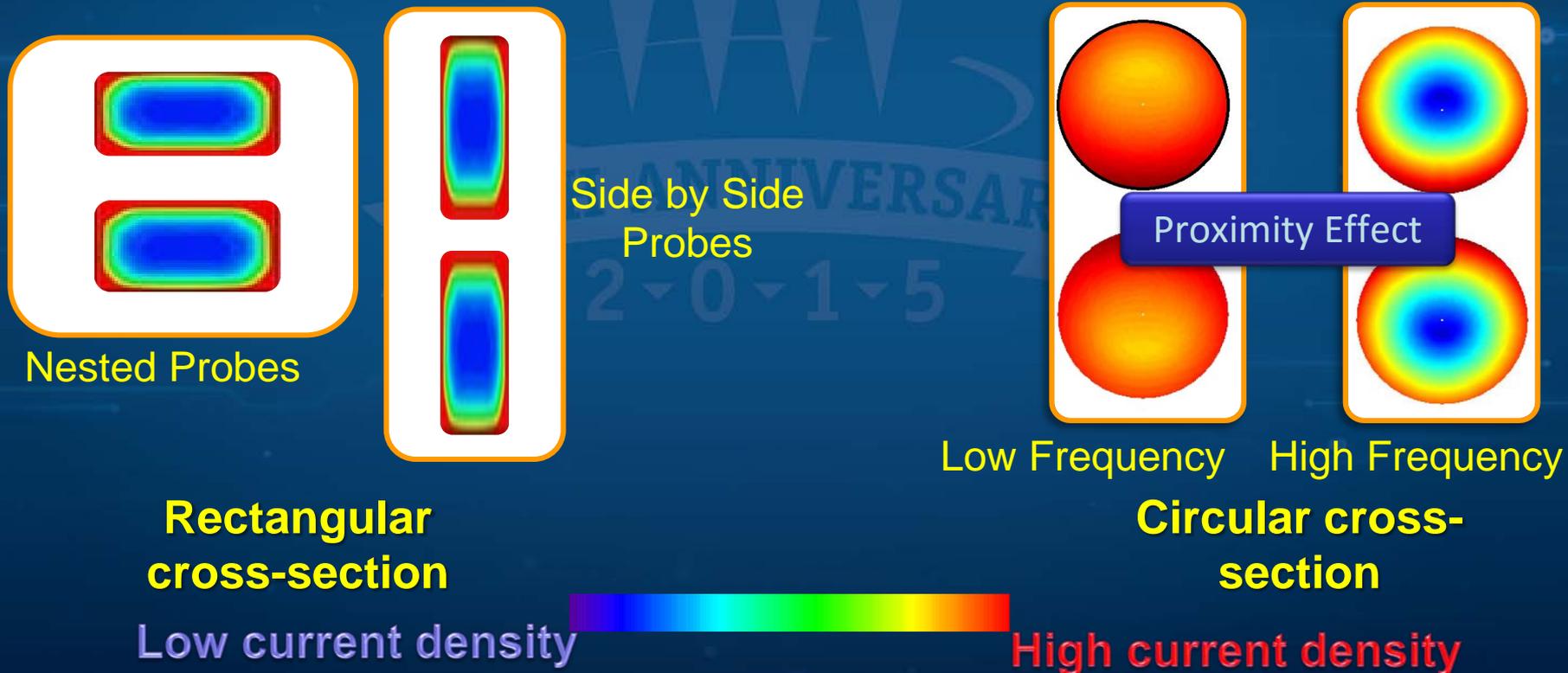


Introduction

Proximity and Skin Effect

Current density distribution in parallel wire.

Unbalanced current distribution due to proximity effect.



Introduction

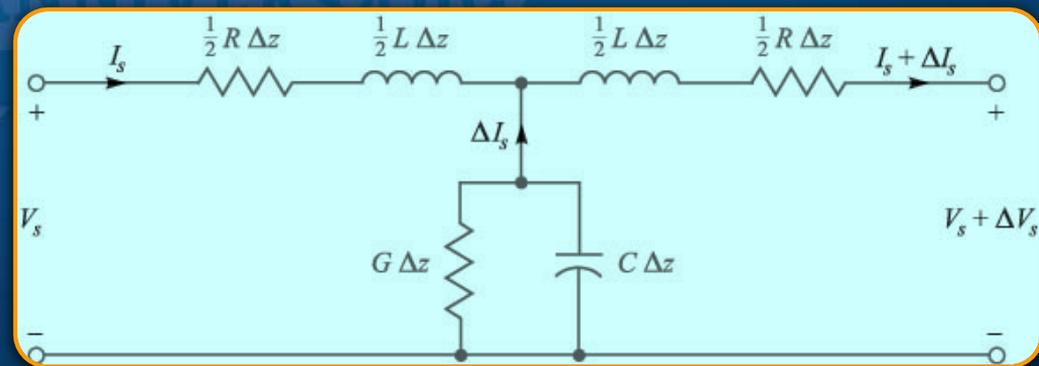
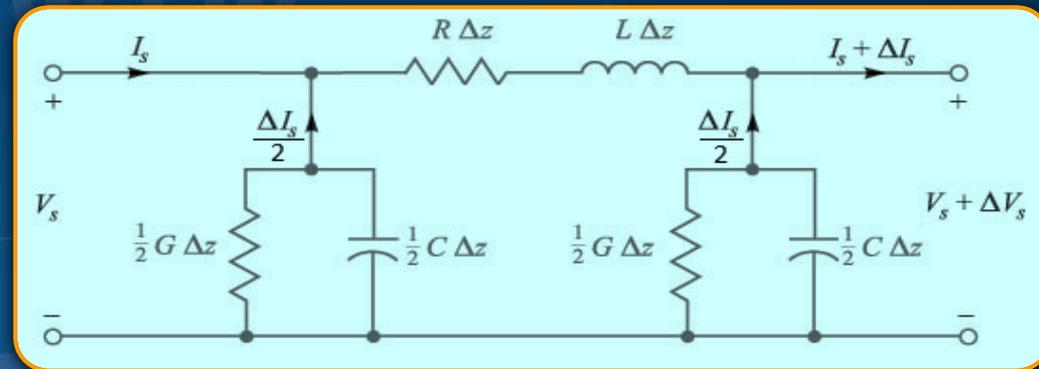
Fundamental Equations

$$L = \frac{\mu}{I_0 I_0^*} \int_s \overline{H} \cdot \overline{H}^* dS$$

$$C = \frac{\varepsilon'}{V_0 V_0^*} \int_s \overline{E} \cdot \overline{E}^* dS$$

$$R = \frac{R_s}{I_0 I_0^*} \oint_{S_1+S_2} \overline{H} \cdot \overline{H}^* dl$$

$$G = \frac{\omega \varepsilon''}{V_0 V_0^*} \int_s \overline{E} \cdot \overline{E}^* dS$$



π and T Equivalent Circuit TL Model

Introduction

Models Comparison

Model	Advantages (Account for)	Disadvantages
Low Frequency	<ul style="list-style-type: none">• Internal and External Inductance• Proximity effect	<ul style="list-style-type: none">• No Skin Effect
High Frequency	<ul style="list-style-type: none">• Skin Effect	<ul style="list-style-type: none">• No Internal Inductance• No Proximity Effect in inductance calculation
Wide Band	<ul style="list-style-type: none">• Skin Effect• Internal Inductance• Proximity Effect in Inductance Calculation	<ul style="list-style-type: none">• No Proximity Effect on Resistance Calculation Only

Closed Form Circuit Model

Models Comparison for Cylindrical Probe

$$L = \frac{\mu_0}{\pi} \left[\frac{1}{4} + \cosh^{-1} \left(\frac{D}{2a} \right) \right]$$

$$R = \frac{2}{\pi a^2 \sigma_c}$$

Low Frequency

$$L_{ext} = \frac{\mu_0}{\pi} \cosh^{-1} \left(\frac{D}{2a} \right)$$

$$R = \frac{R_s}{\pi a} \frac{D/2a}{\sqrt{(D/2a)^2 - 1}}$$

High Frequency

$$L = \text{Im}(Z)$$

$$R = \text{Re}(Z)$$

Wide Band

Where

$$Z = 2Z_{int} + j\omega L_{ext}$$

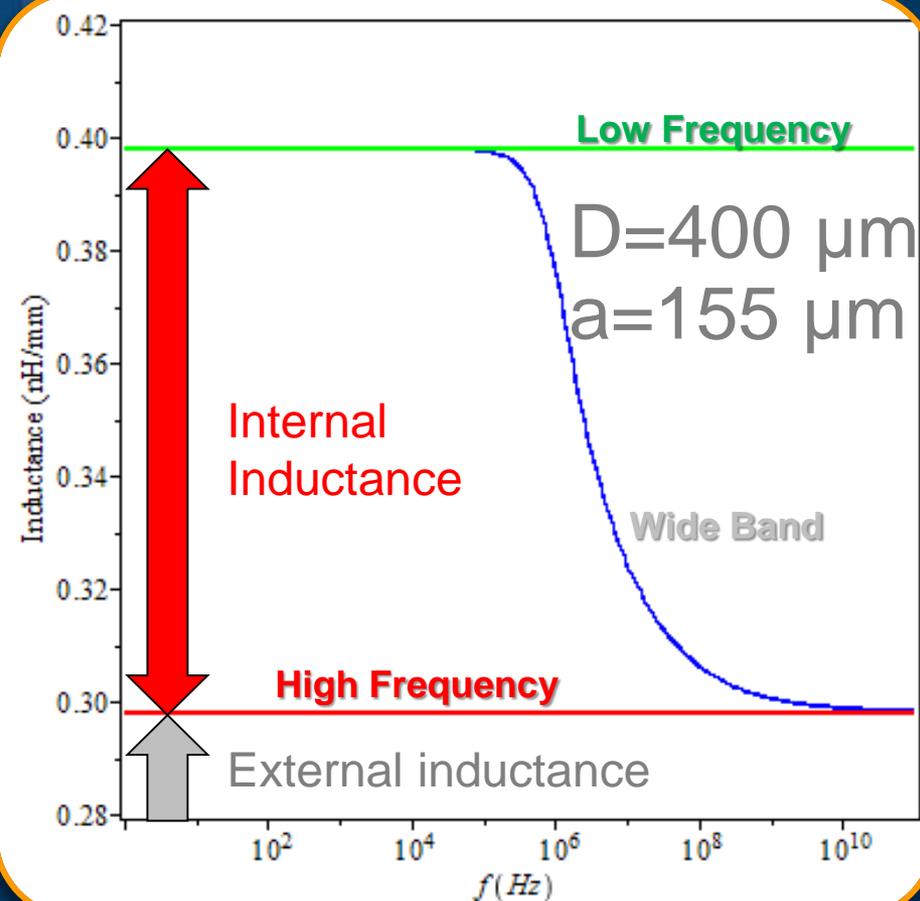
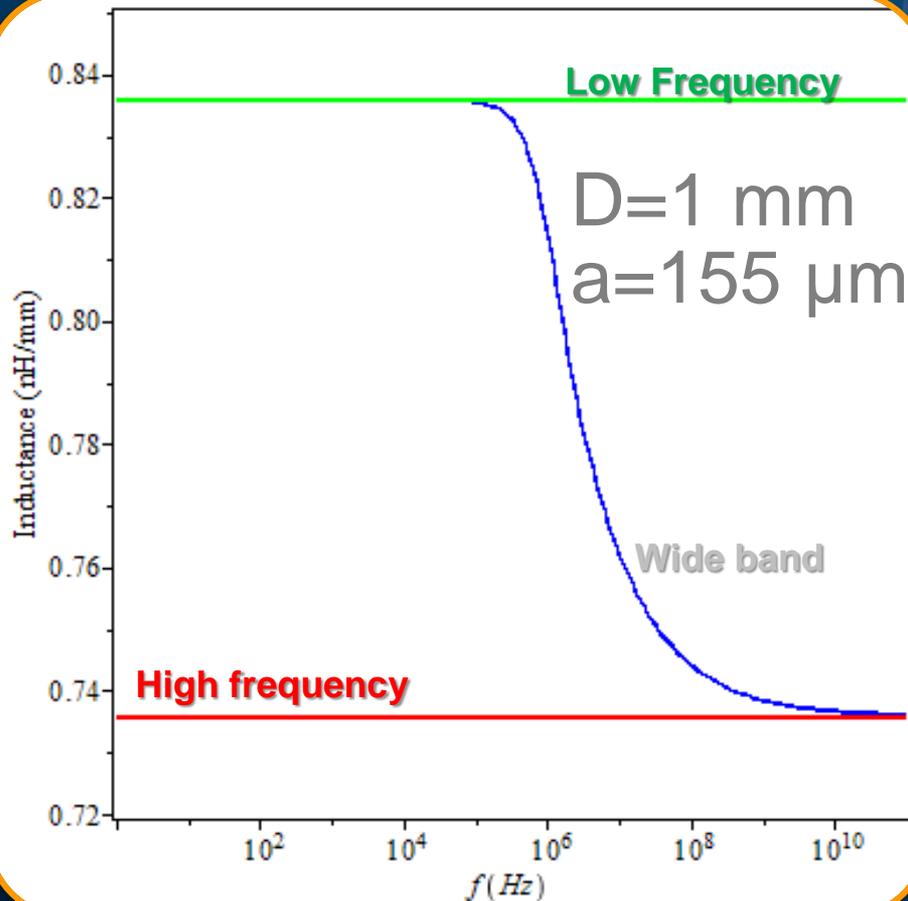
$$Z_{int} = \frac{R_s}{\sqrt{2\pi a}} \frac{ber(\zeta) + jbei(\zeta)}{bei'(\zeta) - jber'(\zeta)}$$

$$L = \frac{R_s}{\pi a} \frac{ber(\zeta)ber'(\zeta) - jbei(\zeta)bei'(\zeta)}{\sqrt{2\omega} \left([bei'(\zeta)]^2 + [ber'(\zeta)]^2 \right)} + \frac{\mu_0}{\pi} \cosh^{-1} \left(\frac{D}{2a} \right)$$

$$R = \frac{R_s}{\pi a} \frac{ber(\zeta)bei'(\zeta) - jbei(\zeta)ber'(\zeta)}{\sqrt{2} \left([bei'(\zeta)]^2 + [ber'(\zeta)]^2 \right)}$$

Closed Form Circuit Model

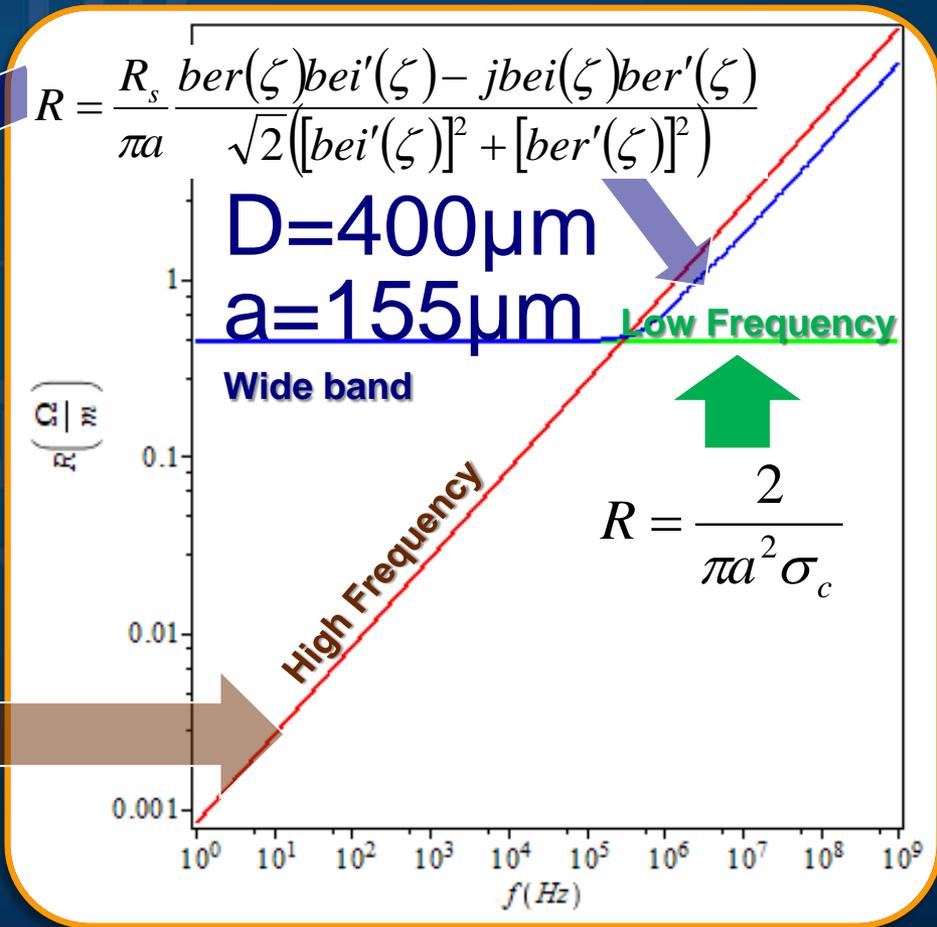
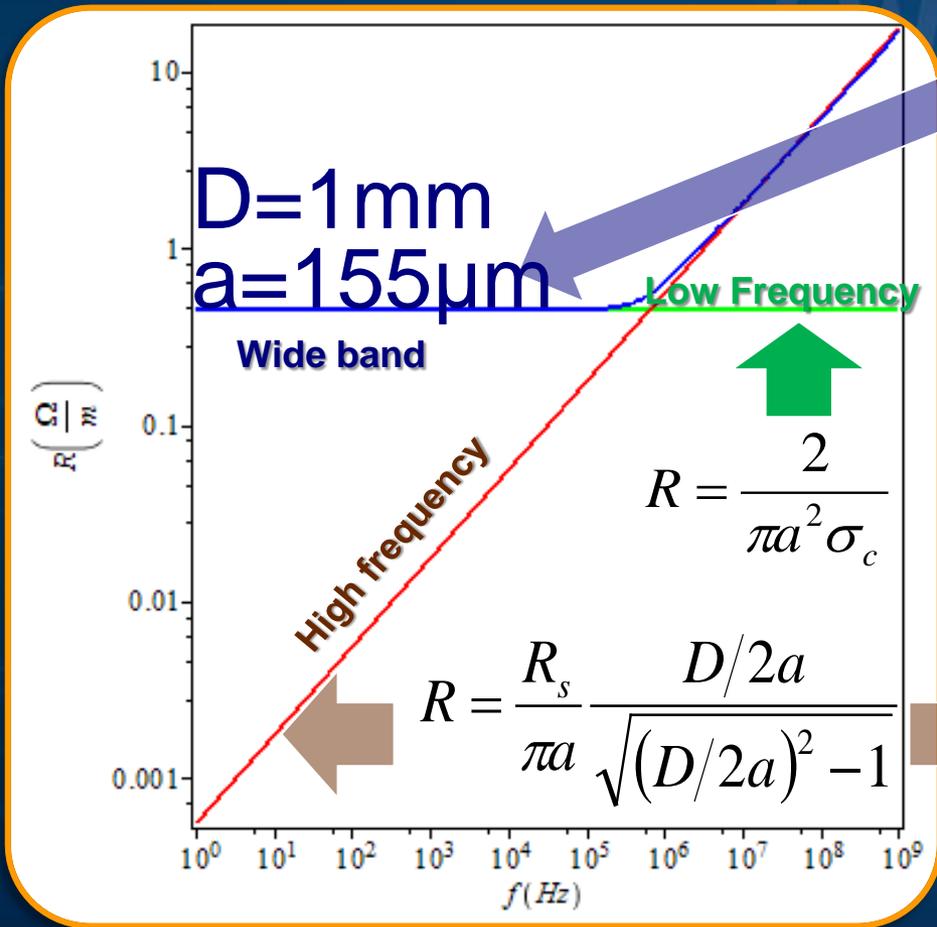
Inductance Comparison for Cylindrical Probe



Calculated based on spring pin dimensions

Closed Form Circuit Model

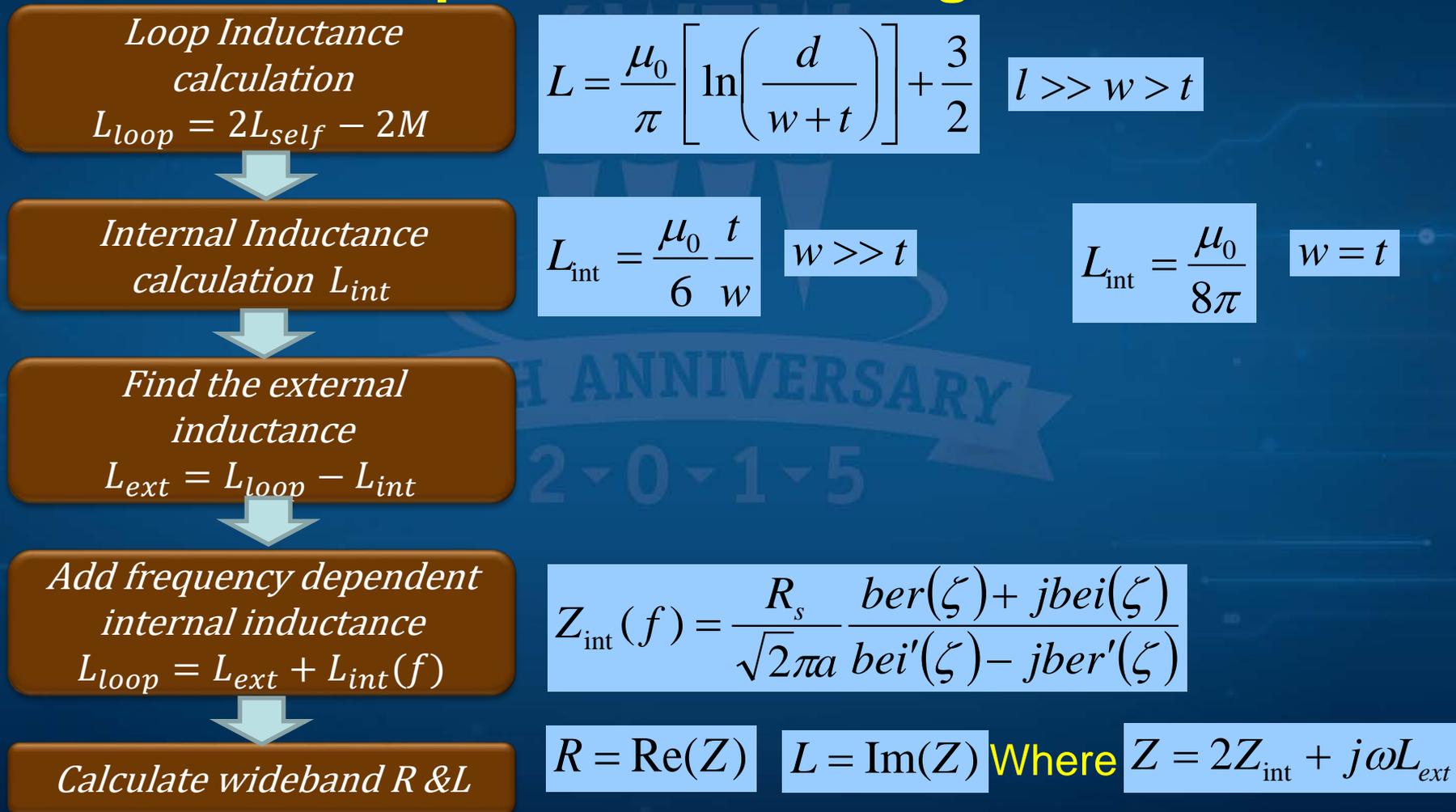
Resistance Comparison for Cylindrical Probe



Calculated based on spring pin dimensions

Closed Form Circuit Model

Models Development for Rectangular Probe



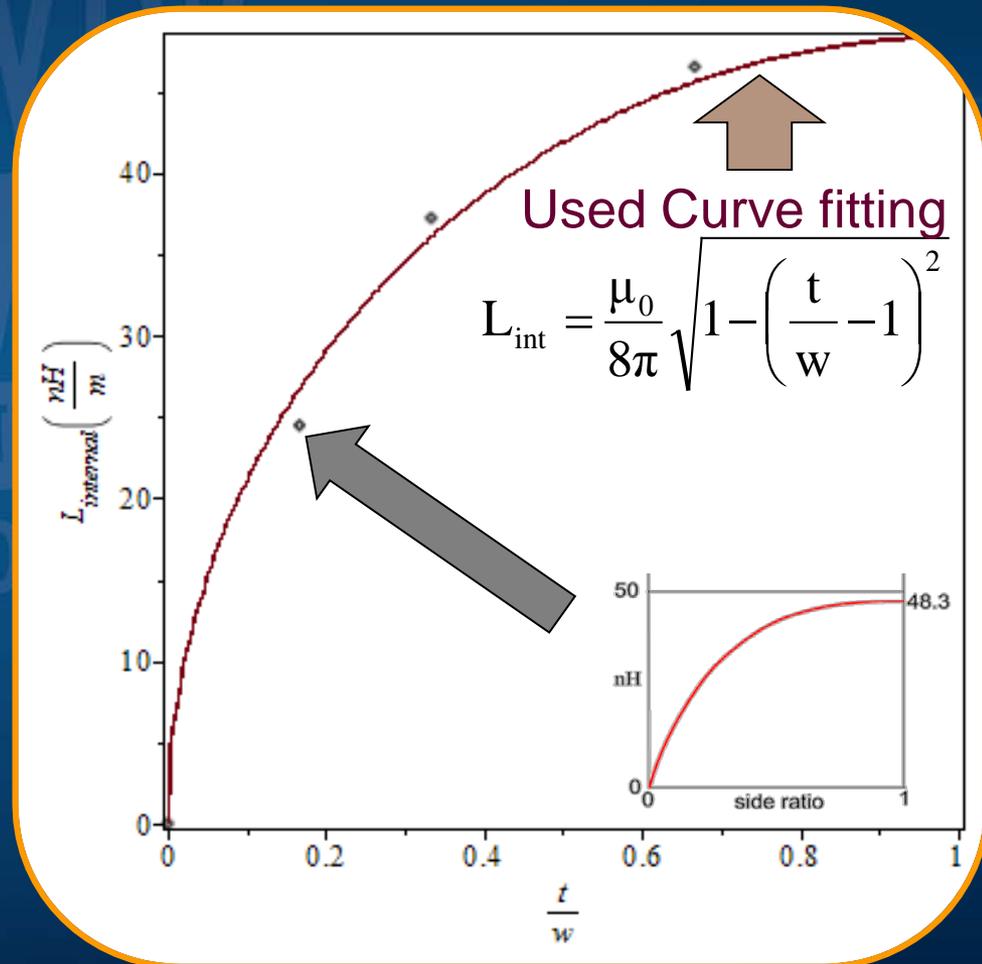
Closed Form Circuit Model

Internal Inductance Correction Factor for Stamped Probe

Nested Probe

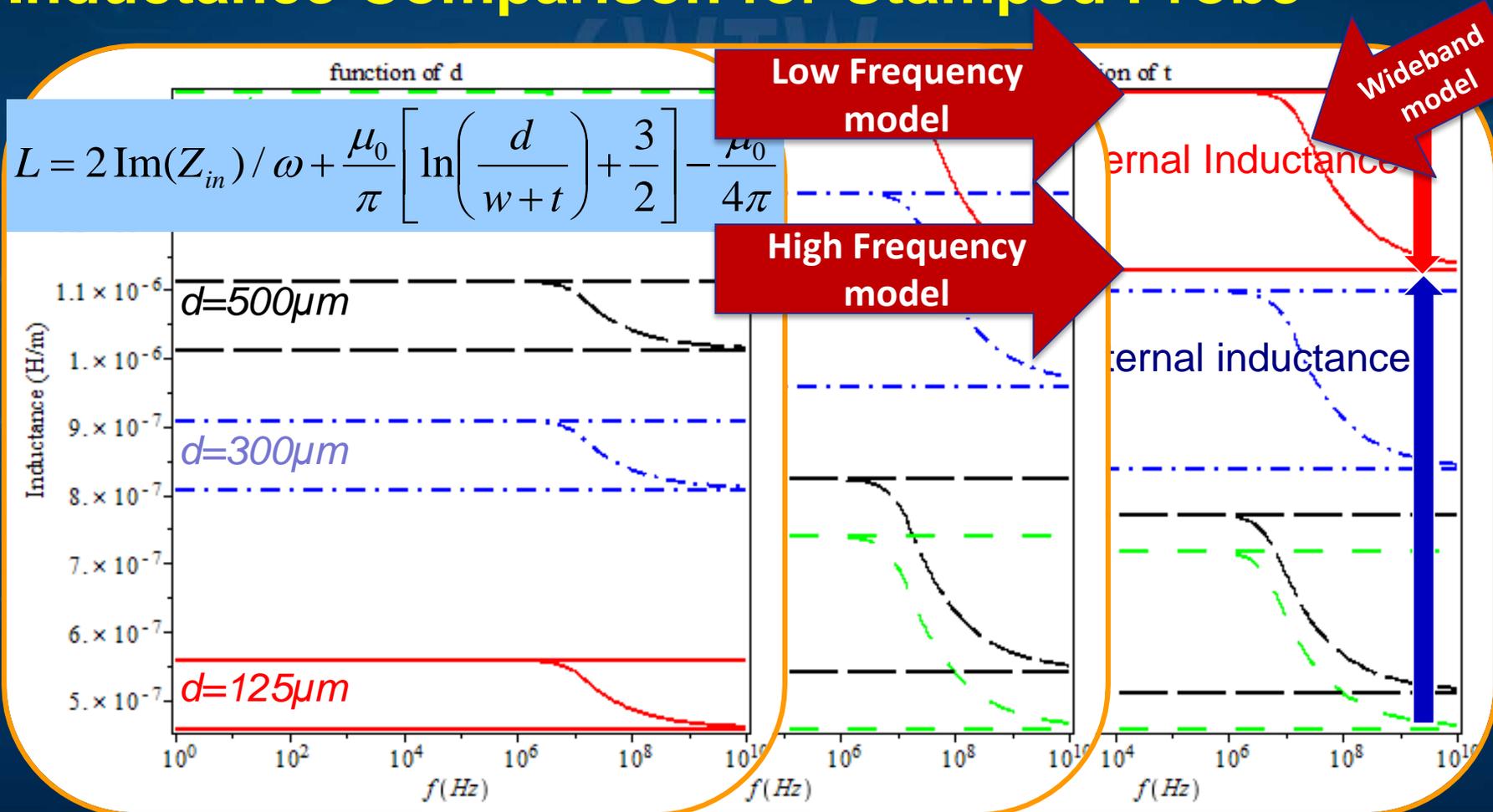


Side by side Probe



Closed Form Circuit Model

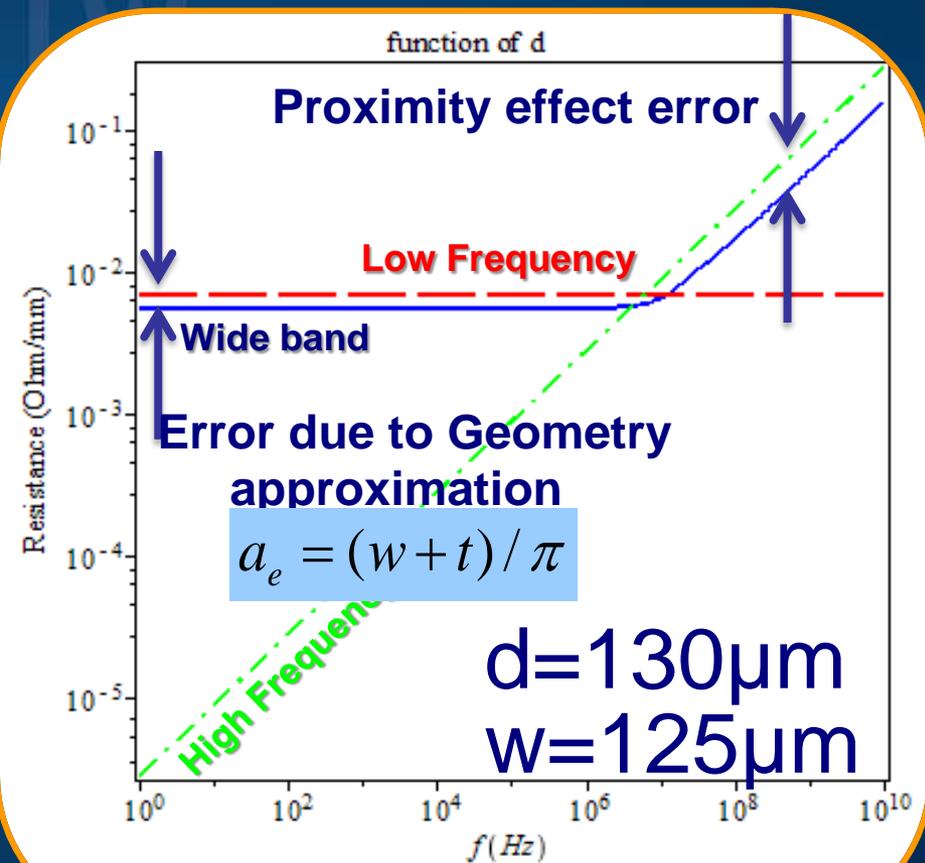
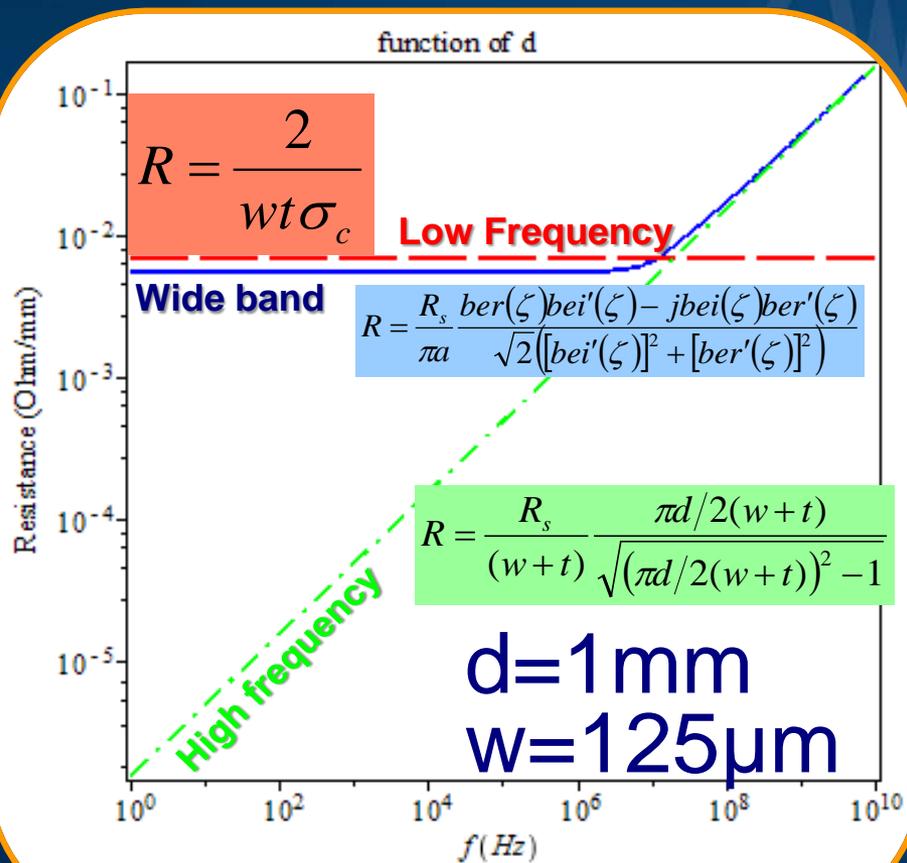
Inductance Comparison for Stamped Probe



Calculated based on 3mil Trio-probe dimensions

Closed Form Circuit Model

Resistance Comparison for Stamped Probe



Calculated based on 3mil Trio-probe dimensions

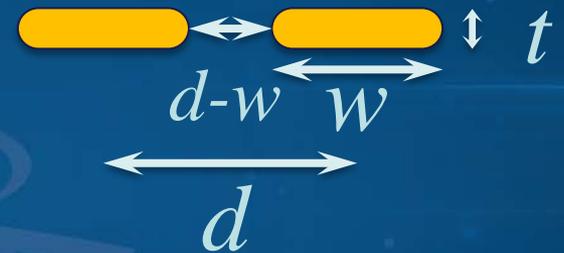
Closed Form Circuit Model

Capacitance Calculation for Stamped Probe

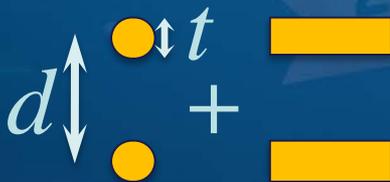
Nested Probe



Side by side Probe



Equivalent

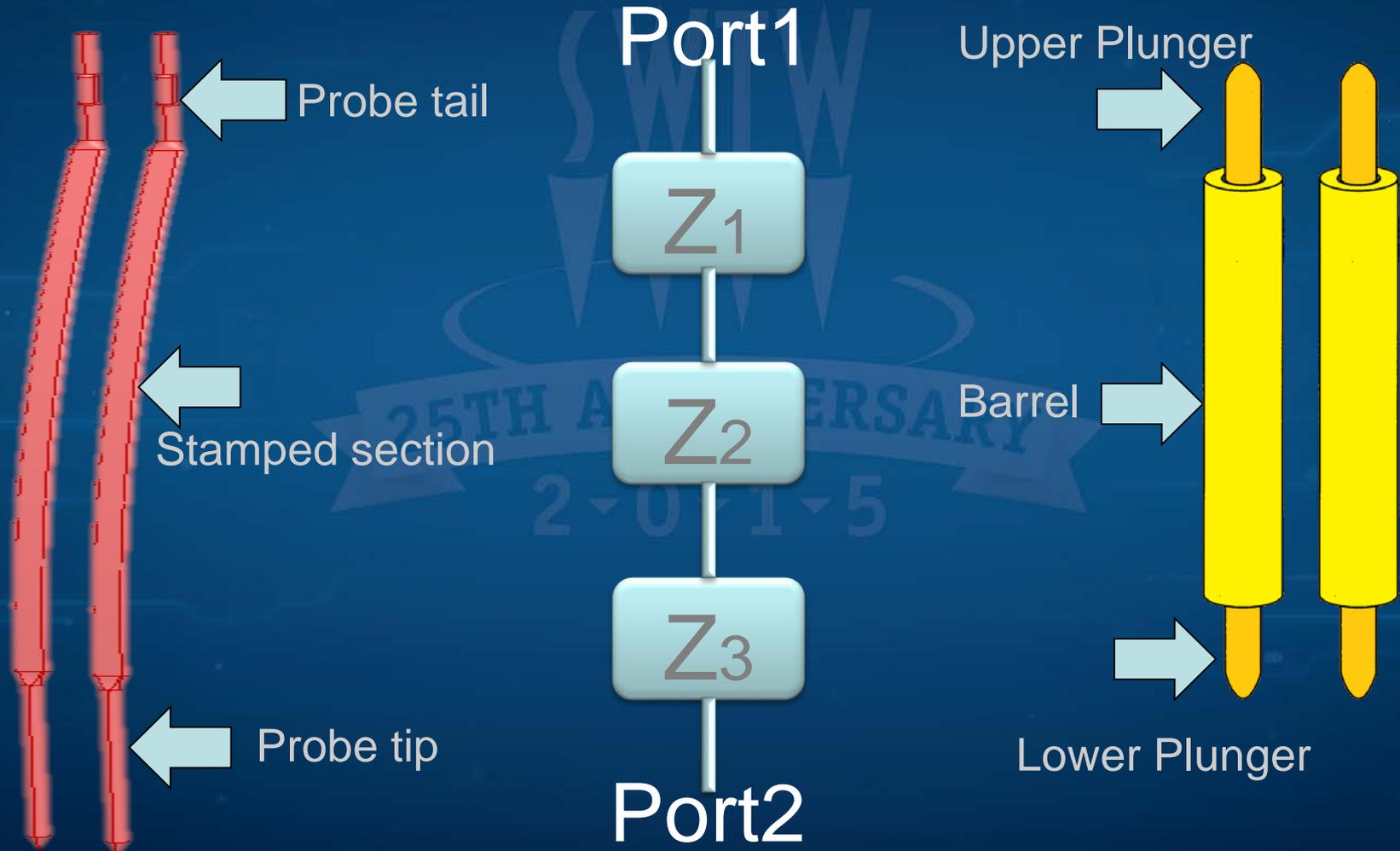


$$C = C_{pp} + C_{fringe} = \frac{w\epsilon}{(d)} + \frac{\pi\epsilon}{\cosh^{-1}(d/t)}$$

$$C = \frac{\pi\epsilon}{\cosh^{-1}((d-w+t)/t)}$$

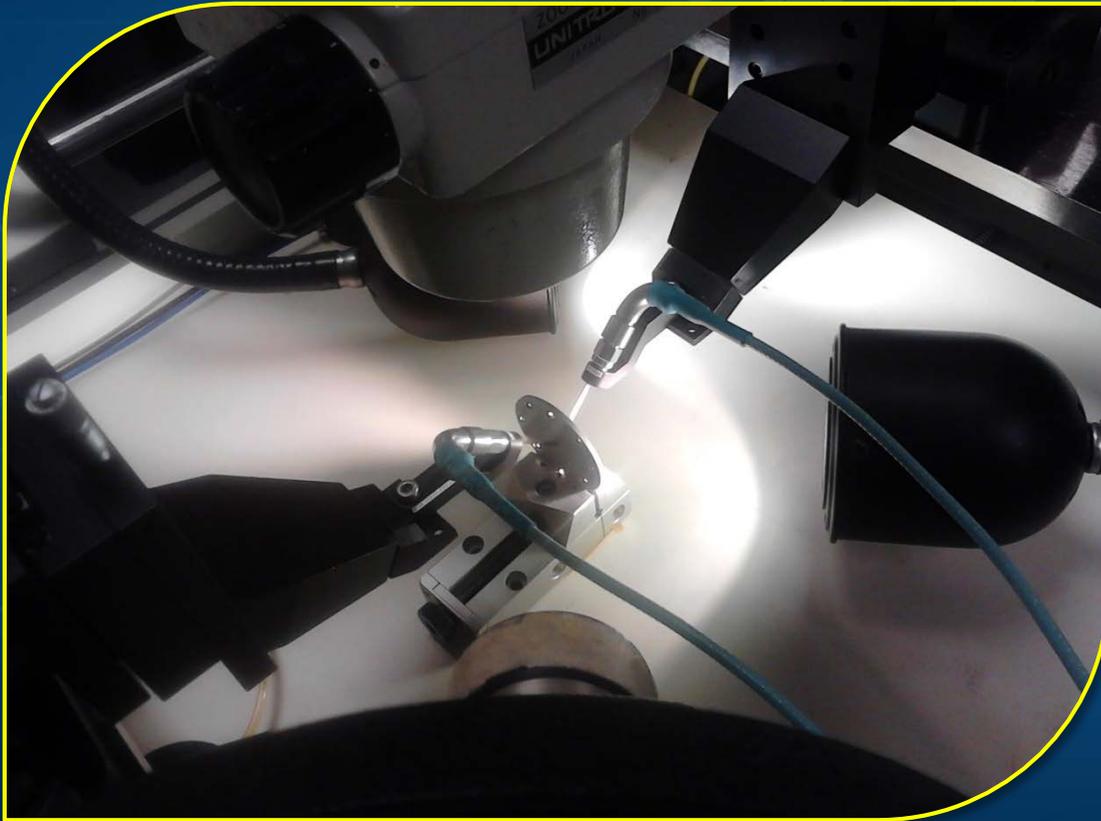
Closed Form Circuit Model

Circuit Model



Measurements & Simulation

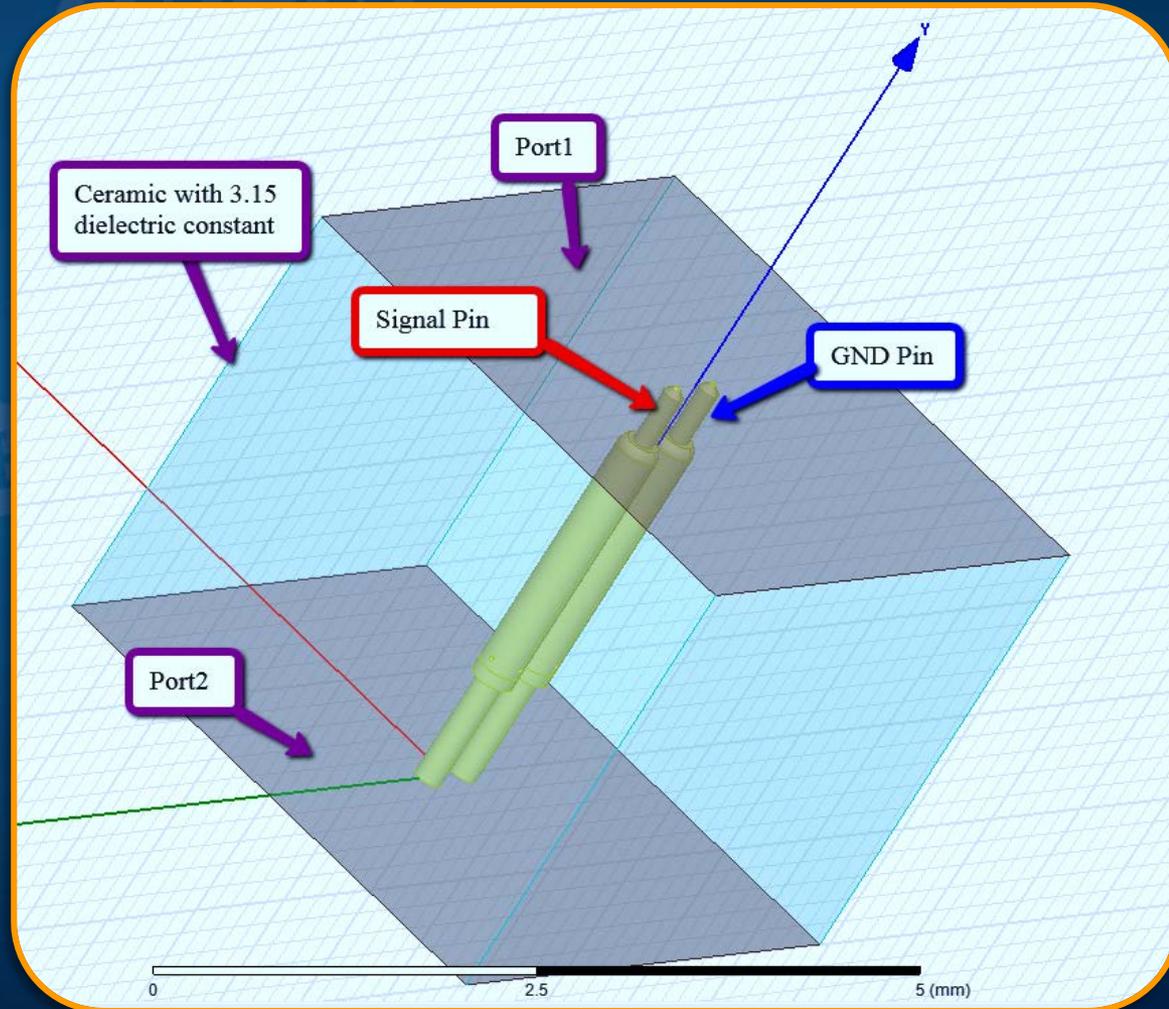
Measurement Setup



Measurements & Simulation

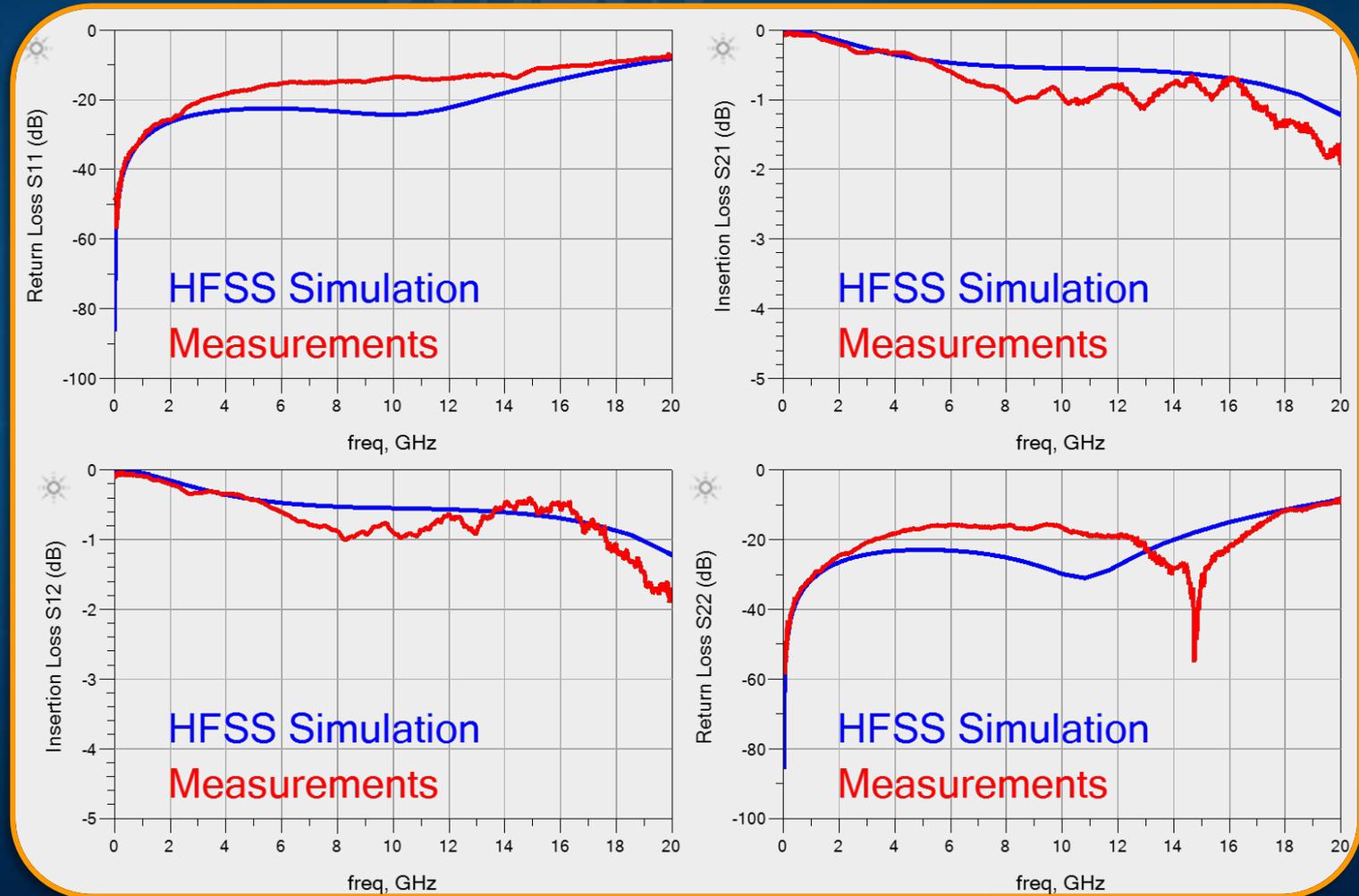
Ansoft HFSS Simulation

Structure and
Boundary
conditions.



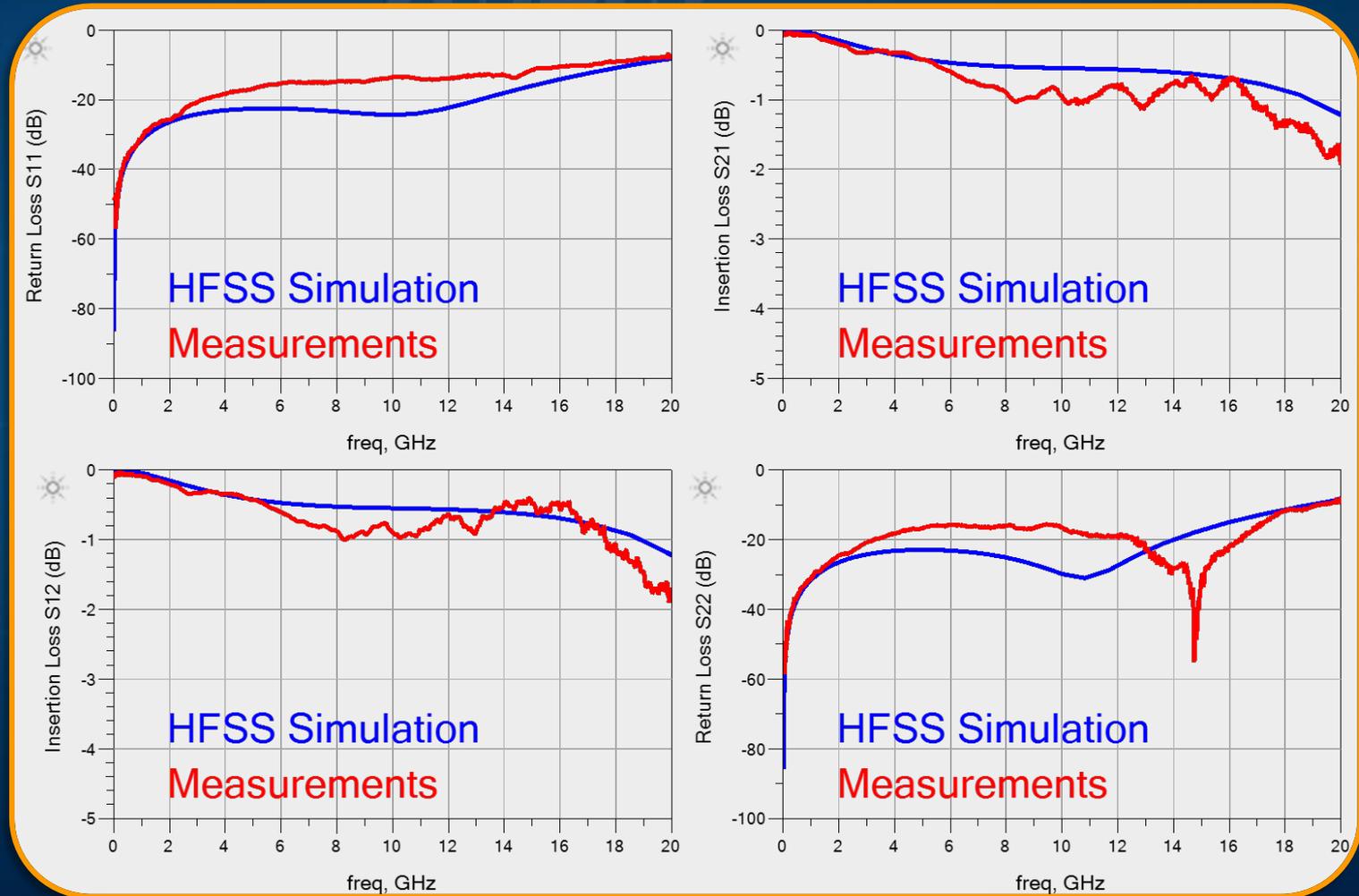
Measurements & Simulation

Insertion and Return Loss Magnitude



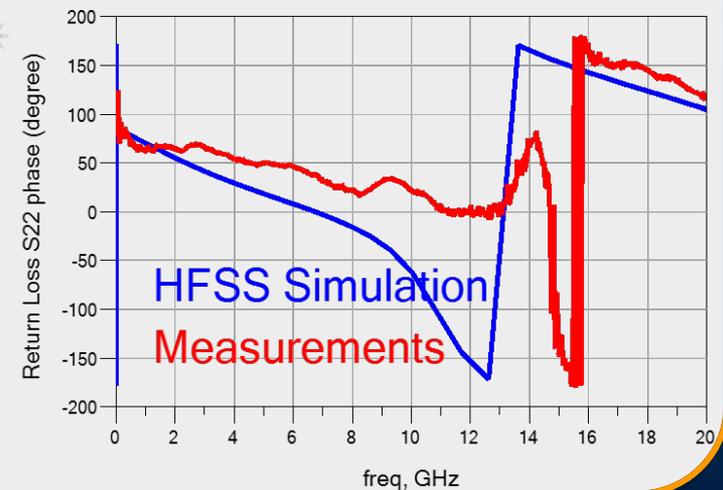
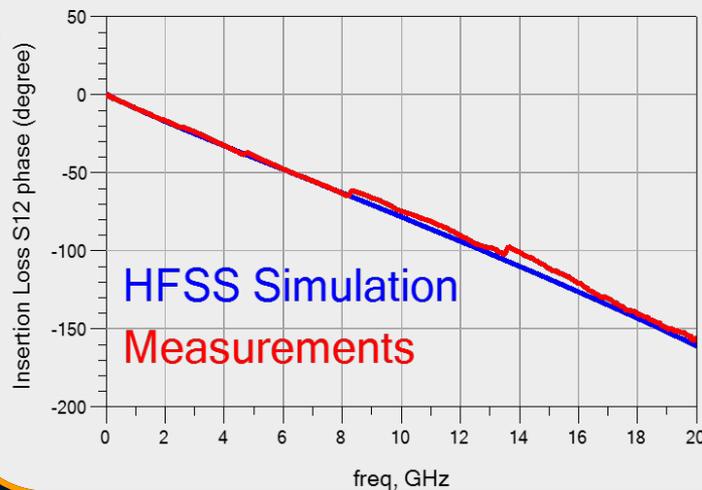
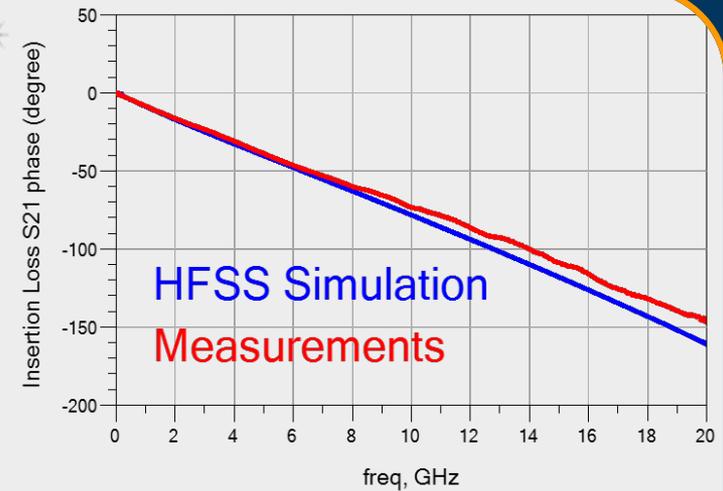
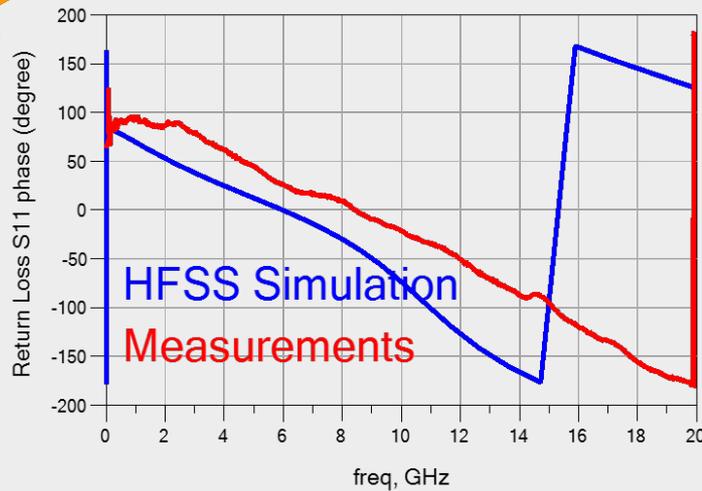
Measurements & Simulation

Insertion and Return Loss Magnitude



Measurements & Simulation

Insertion and Return Loss Phase



Circuit Model & Model Verification

Lumped Circuit π Model

Upper Plunger

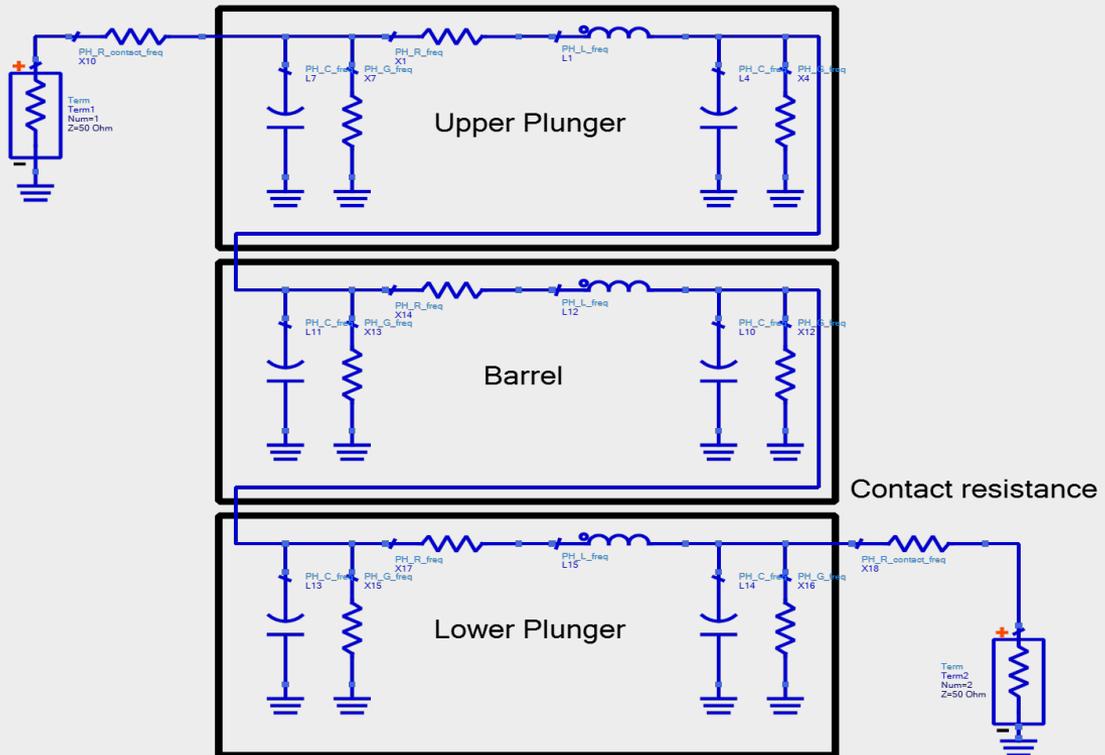
Barrel

Lower Plunger

S-PARAMETERS

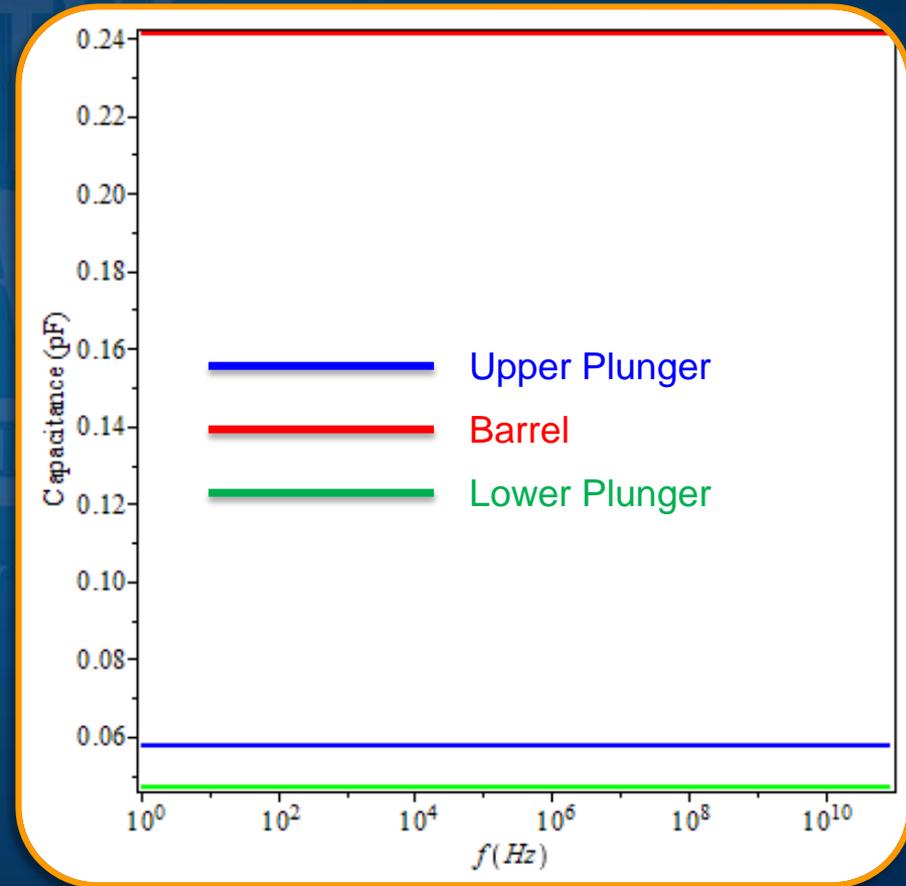
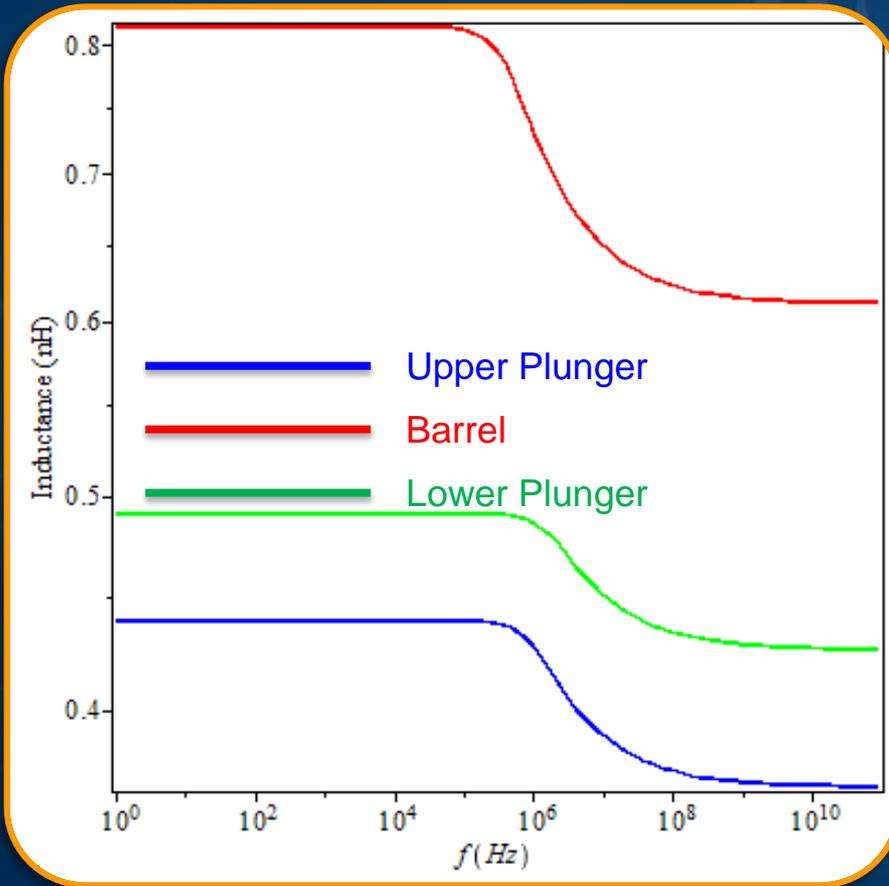
S_Param
SP1
Start=1.0 Hz
Stop=20 GHz
Step=

Contact resistance



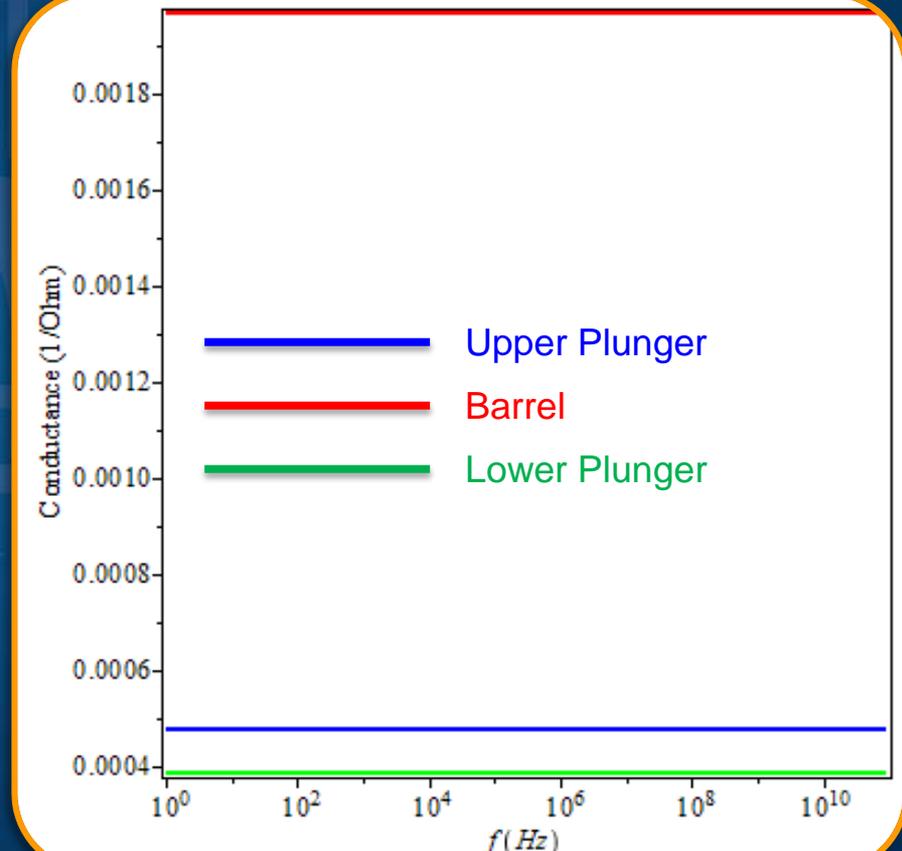
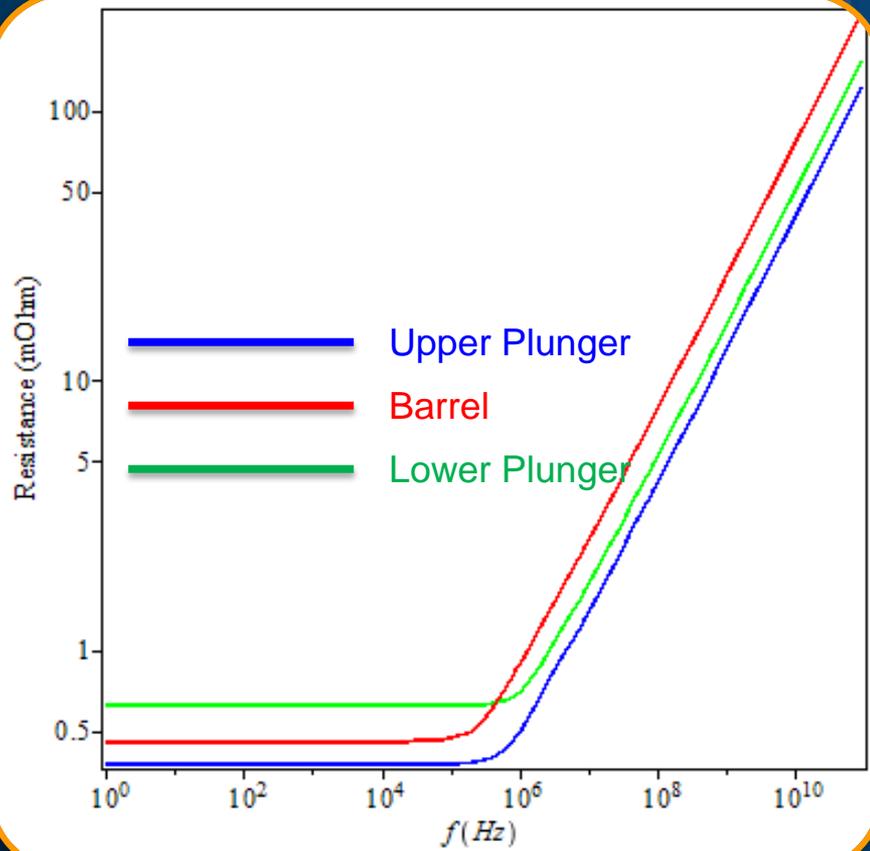
Circuit Model & Model Verification

Circuit Model Parameters (Total L & C)



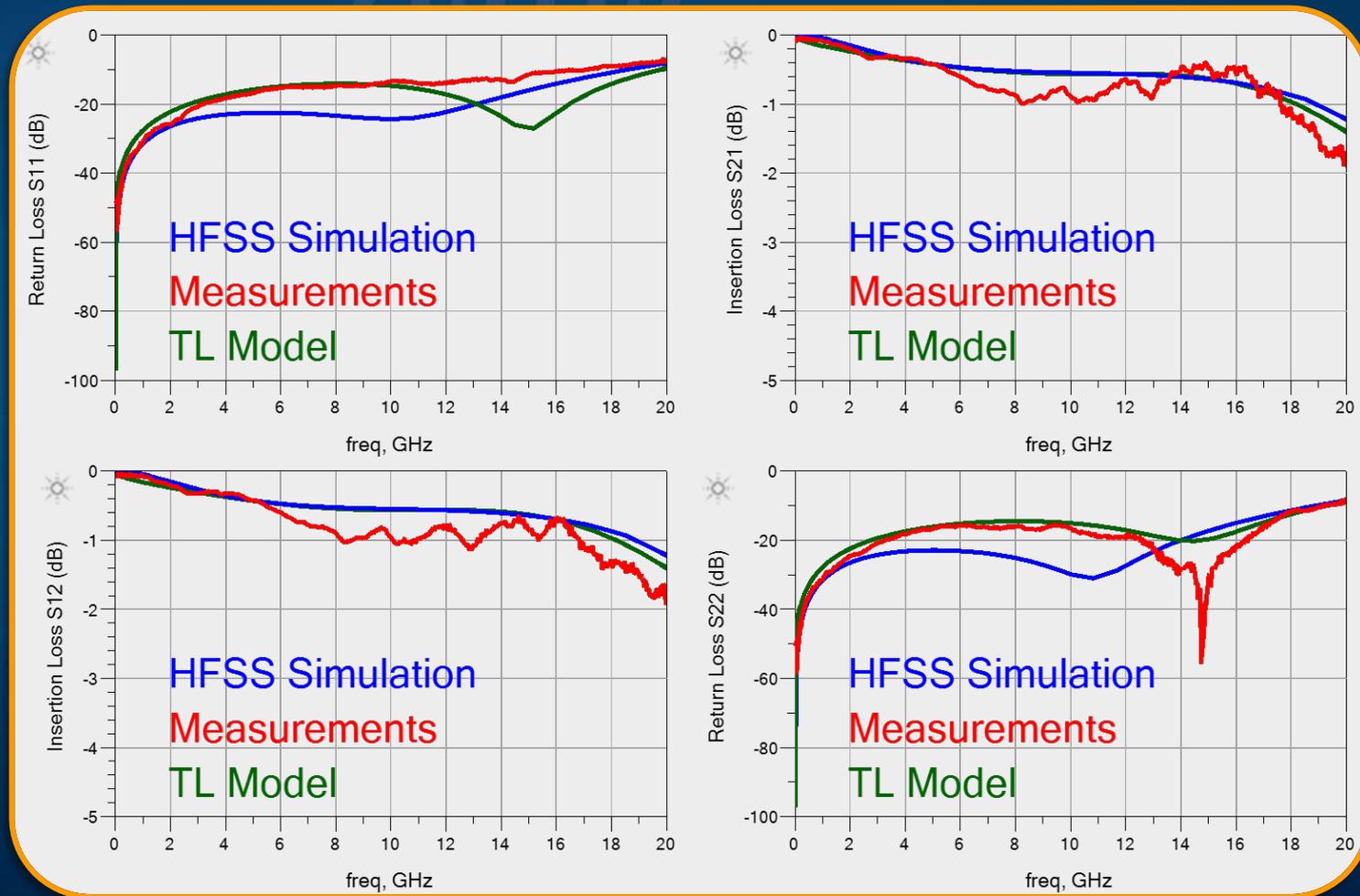
Circuit Model & Model Verification

Circuit Model Parameters (total R & G)



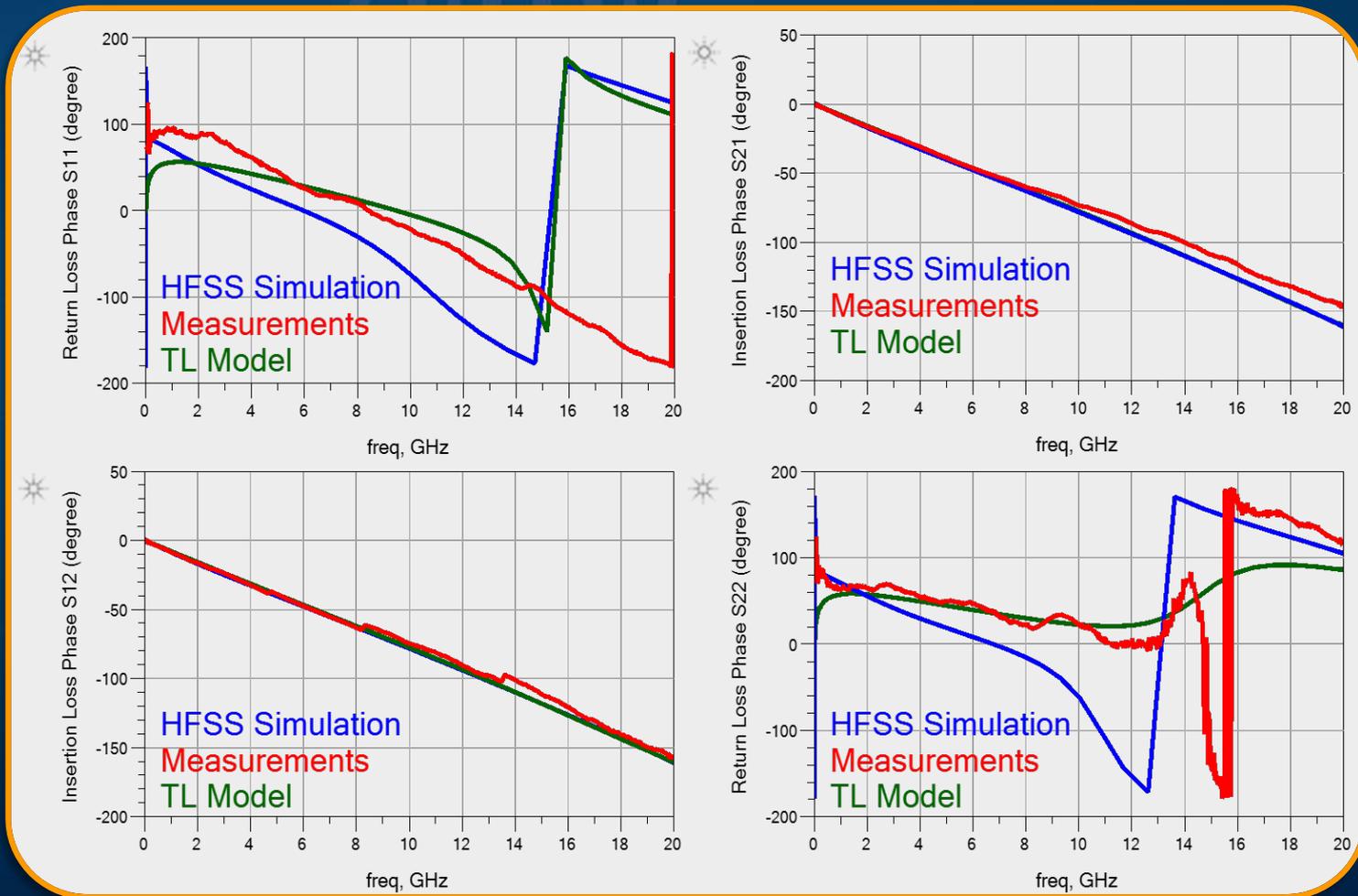
Circuit Model & Model Verification

TL Circuit Model S-Parameters



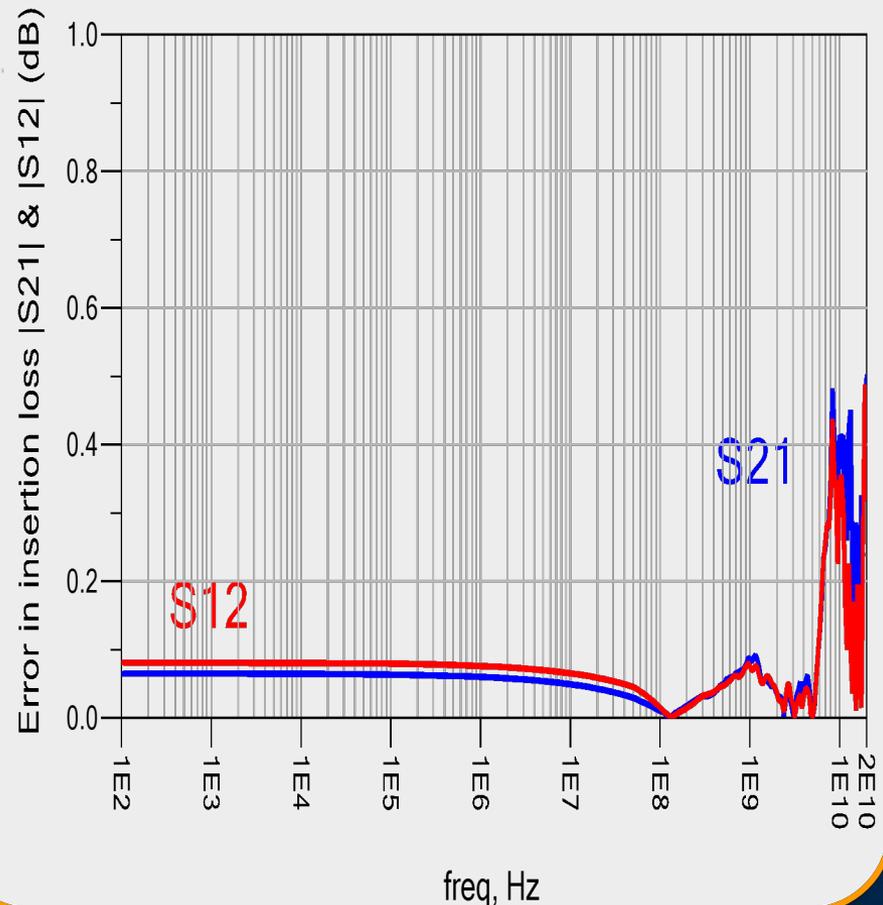
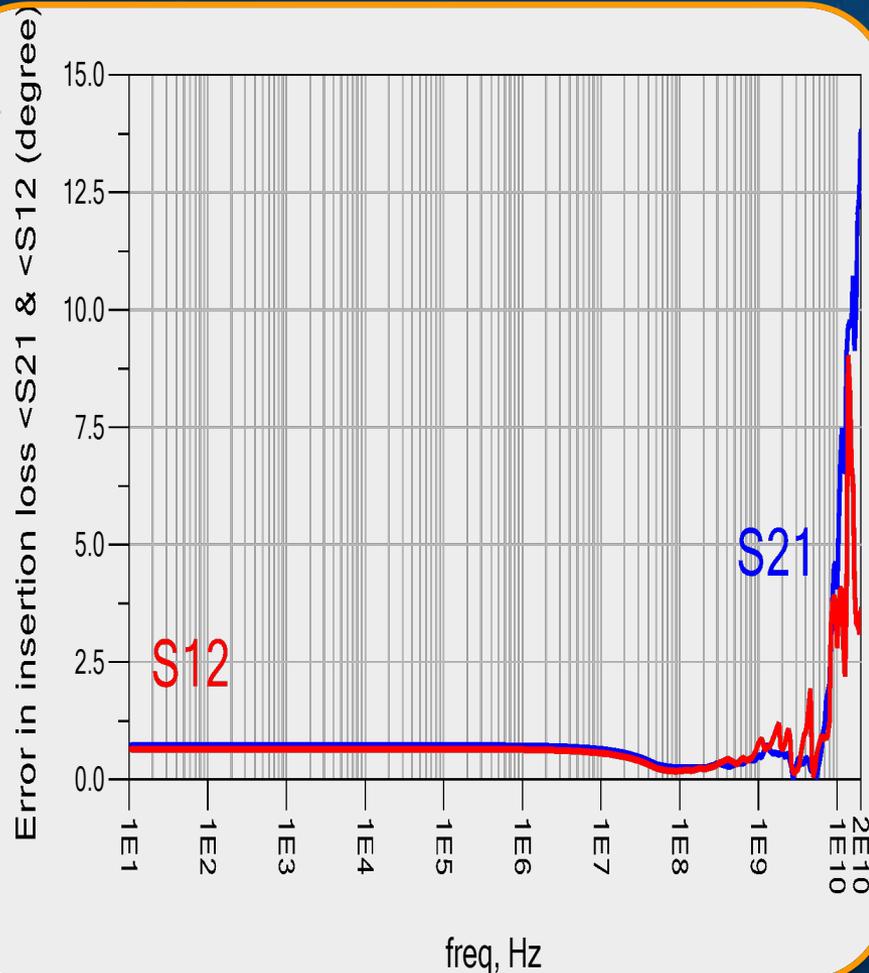
Circuit Model & Model Verification

TL Circuit Model S-Parameters



Circuit Model & Model Verification

Measurements vs. Model Magnitude & Phase



SUMMARY

- Lumped and TL circuit models had been developed using close form Wideband solution.
- Two models were developed. One for circular cross section and one for rectangular cross section
- Models had been analyzed for 400um probe spacing.
- Models were verified against Spring pin measurements and field analysis simulation results.
- Results show a good match with maximum magnitude error of 0.5dB and phase error of 12 degree at high frequency

CONCLUSION

- Using a closed form model, minimize simulation time and cost.
- Closed form model can be used for quick product feasibility
- Model can be integrated with other probe card components to obtain a full performance prior to manufacturing to minimize risks and design optimization time delays.
- TL model provides better results compared with lumped circuit model, where distribution effect takes place.

References

- Utkarsh R. Patel, Bjrn Gustavsen, and Piero Triverioyz, “An Equivalent Surface Current Approach for the Computation of the Series Impedance of Power Cables with Inclusion of Skin and Proximity Effects”, IEEE Transactions On Power Delivery, 15 August 2013
- C. R. Paul, Analysis of Multiconductor Transmission Lines, 2nd ed., Wiley, 2007.
- M. M. Al-Asadi, A. P. Duffy, A. J. Willis, K. Hodge, and T. M. Benson, “A Simple Formula For Calculating The Frequency-dependent Resistance Of A Round Wire”, Microwave And Optical Technology Letters, Vol. 19, No. 2, October 5 1998
- Pagnetti, A., Xemard, A., Paladian, F., and Nucci, “Evaluation of the impact of proximity effect in the calculation of the internal impedance of cylindrical conductors”, URSI 2011, Aug. 2011.
- C.L. Holloway and E.F. Kuester, "DC Internal Inductance for a Conductor of Rectangular Cross Section", IEEE Transactions on Electromagnetic Compatibility, Vol. 51, No. 2, pp. 338-344, May 2009.
- Z. Piatek, and B. Baron, “Exact closed form formula for self inductance of conductor of rectangular cross section”, Progress In Electromagnetics Research M, Vol. 26, 225-236, 2012
- van der Meijs, N. P.; Fokkema, J. T., “VLSI Circuit Reconstruction From Mask Topology Integration”, VLSI Journal,1984, 2, 85-119.